# The New Priority Ranking Systems for Man-made Slopes and Retaining Walls

**GEO Report No. 284** 

P.F.K. Cheng

Geotechnical Engineering Office Civil Engineering and Development Department The Government of the Hong Kong Special Administrative Region

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## **Preface**

In keeping with our policy of releasing information which may be of general interest to the geotechnical profession and the public, we make available selected internal reports in a series of publications termed the GEO Report series. The GEO Reports can be downloaded from the website of the Civil Engineering and Development Department (http://www.cedd.gov.hk) on the Internet. Printed copies are also available for some GEO Reports. For printed copies, a charge is made to cover the cost of printing.

The Geotechnical Engineering Office also produces documents specifically for publication in print. These include guidance documents and results of comprehensive reviews. They can also be downloaded from the above website.

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H.N. Wong Head, Geotechnical Engineering Office August 2013

#### **Foreword**

The Government has launched the Landslip Prevention and Mitigation Programme (LPMitP) on a rolling basis to dovetail with the Landslip Preventive Measures (LPM) Programme upon its completion in 2010, to deal with landslide risks associated with the remaining man-made slope features and vulnerable natural hillside catchments.

This report documents the risk-based New Priority Ranking Systems (NPRS) which have been developed by the Geotechnical Engineering Office (GEO) to allow the ranking of both pre-1978 and post-1978 man-made slopes and retaining walls for priority attention under the LPMitP. The NPRS supersede the New Priority Classification Systems (NPCS), which were previously developed by the GEO for dealing with the high-risk old (i.e. pre-1978) man-made slope features under the 10-year (2000-2010) Extended LPM Programme.

The NPRS were jointly developed by Dr Dominic O.K. Lo, Ms Patty F.K. Cheng, Mr W.K. Pun and Mr Anthony Y.T. Lam.

A draft of the NPRS was reviewed by the Slope Safety Technical Review Board (SSTRB) comprising Dr Suzanne Lacasse, Professor Oldrich Hungr and Professor Wang Si-Jing, and their comments and suggestions were incorporated into the NPRS.

This report was compiled by Ms Patty F.K. Cheng under the supervision of Mr Anthony Y.T. Lam.

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#### **Abstract**

This report documents the New Priority Ranking Systems (NPRS) for man-made slopes and retaining walls. The NPRS are risk-based ranking systems that consider both the likelihood and consequence of slope failures. The NPRS have been developed by the Geotechnical Engineering Office for the individual feature types (viz. soil cut slopes, rock cut slopes, fill slopes and retaining walls) to allow the priority ranking of both pre-1978 and post-1978 man-made slope features under the post-2010 Landslip Prevention and Mitigation Programme (LPMitP).

The likelihood of slope failures is reflected by an Instability Score, while the consequence of failure is reflected by a Consequence Score. The risk of slope failures is reflected by a Total Score, which is computed as the product of the Instability Score and the Consequence Score.

Instability Score accounts for the instability potential of a slope feature and its actual performance. The instability potential is assessed by considering the key factors that affect the likelihood of failure. The actual slope performance is manifested as signs of distress where present and records of instability after the slope feature has been formed or treated to its present configuration.

Consequence Score considers the facilities affected in the event of a slope failure. It takes due account of the type and proximity of the affected facilities, scale and mechanism of failure, together with the topography adjacent to the slope features.

A methodology for combining the Total Score computed by the individual NPRS is formulated based on the overall risk distribution of the four respective types of slope features, namely soil cut slopes, rock cut slopes, fill slopes and retaining walls. The resultant Ranking Score is unique for each slope feature and can be used for selection of deserving man-made slope features for follow-up action under the LPMitP.

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#### 1 Introduction

This report documents the New Priority Ranking Systems (NPRS) which have been developed by the Geotechnical Engineering Office (GEO) for slope selection under the Landslip Prevention and Mitigation Programme (LPMitP). With the completion of the Landslip Preventive Measures (LPM) Programme by 2010, all the high-risk old (i.e. pre-1978) man-made slope features affecting major roads and developments will have been dealt with. To dovetail with the LPM Programme, the Government has launched the LPMitP on a rolling basis, in order to contain the landslide risks associated with the remaining man-made slope features and vulnerable natural hillside catchments.

Apart from vulnerable natural hillsides, the LPMitP primarily targets man-made slope features that are of moderate risk, viz. old slopes affecting frequently used road, footpaths, public waiting areas, etc. and post-1978 slopes formed or treated over 20 years ago with non-robust technology, which are denoted as "old technology" slopes<sup>1</sup>. The NPRS have been formulated for the respective feature types (viz. soil cut slopes, rock cut slopes, fill slopes and retaining walls) to allow the ranking of both pre-1978 and post-1978 man-made slope features for priority attention under the LPMitP. The priority ranking system for vulnerable natural hillside catchments is outside the scope of this report.

This report presents the methodology of the NPRS and gives guidance on collection of field data and computation of scores for man-made slope features. Worked examples are also provided in this report.

## 2 New Priority Ranking Systems

## 2.1 The Systems

The LPM Programme primarily targets high-risk pre-1978 man-made slope features, for which the New Priority Classification Systems (NPCS) were developed by the GEO for priority ranking (Wong, 1998). The LPMitP primarily targets moderate-risk pre-1978 and selected post-1978 man-made slope features. The resolution of the NPCS is not adequate to distinguish the relative risks of a large number of moderate-risk man-made slope features and that the degree of past geotechnical engineering input to post-1978 slopes is not accounted for. Also, further insights have been obtained through GEO's systematic landslide investigation programme (Ho & Pappin, 2007), which have proved useful for refining selected factors and their weightings in the priority ranking systems. In light of the above, new NPRS were developed by the GEO primarily for use under the post-2010 LPMitP.

The NPRS are risk-based ranking systems that consider both the likelihood and the consequence of slope failures. The likelihood of failure is reflected by an Instability Score (*IS*) while the consequence of failure is reflected by a Consequence Score (*CS*). Each system for the four types of slope feature is based on the same equation, which computes a Total Score (*TS*). The *TS* is the product of *IS* and *CS*, i.e.

<sup>&</sup>lt;sup>1</sup> Old technology slopes are formed or treated from 1977 to late 1980s based on knowledge and technology at the time, typically comprise slopes trimmed back to a less steep gradient without the provision of reinforcement or structural support. These slopes are prone to degradation and less robust than those treated with modern technology such as soil nails.

$$TS = IS \times CS$$
 (2.1)

IS accounts for the instability potential of a slope feature and its actual performance. The assessment of Instability Potential (IP) is based on the consideration of a number of key factors that affect the likelihood of failure. The NPRS place due emphasis on the Actual Performance (AP) of a man-made slope feature, which is manifested as signs of distress where present and records of instability after the slope feature has been formed or treated to its present configuration. IS is the product of IP and AP, i.e.

$$IS = IP \times AP \dots (2.2)$$

Factors contributing to the *IP* are different for the individual feature types due to the fact that their failure mechanisms, together with the causes and triggering factors of failure, are not the same. Factors considered in each system are addressed in Sections 3 to 6.

Signs of distress of a slope feature are classified into three levels (i.e. severe, moderate and minor). Guidelines on the classification of signs of distress for the individual ranking systems are given in Appendices A to D.

CS reflects the severity of the consequence of a slope failure in terms of the potential loss of life. It takes due account of the type and proximity of the affected facilities, scale and mechanism of failure, and the topography adjacent to the slope features. The proximity of the toe facilities and the topography adjacent to the slope feature is accounted for by the shadow angle  $(\omega)$ , see Figure 2.1.

In the NPRS, the types of facilities affected are subdivided into five facility groups, pursuant to GEO Technical Guidance Note (TGN) No. 15 (GEO, 2007). The consequence-to-life categories corresponding to the different facilities are presented in Table 2.1.

Roads should be classified as the appropriate facility groups based on the most recent Annual Average Daily Traffic (AADT) and the number of traffic lanes (see Figure 2.2). The AADT data for a vast majority of roads in Hong Kong are available in the Annual Traffic Census published by the Transport Department.

It should be noted that the NPRS take account of direct-risk-to-life only, i.e. the consideration of indirect risk-to-life is excluded. Also, the following categories of slope feature will not be ranked for action under the LPMitP:

- (a) Government soil cut slopes that were formed/treated in or after year 2000, and processed and accepted by GEO.
- (b) Government soil cut slopes that were treated with robust technology<sup>2</sup> (e.g. installed with soil nails), and processed and accepted by GEO.

<sup>&</sup>lt;sup>2</sup> Robust technology refers to those design solutions that are not unduly sensitive to uncertainties associated with locally adverse geological and hydrogeological conditions (Ho et al, 2003). For example, soil nailing is a robust technology in the case of soil cut slopes.

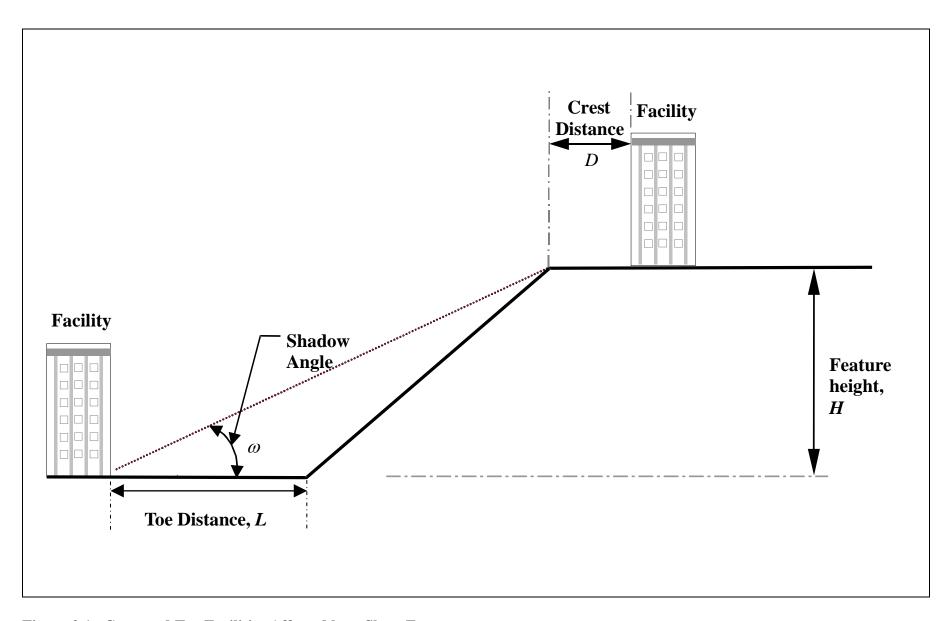


Figure 2.1 Crest and Toe Facilities Affected by a Slope Feature

Table 2.1 Typical Examples of Facilities under Different Facility Groups Affected by Landslides

Facility Group		Facilities	Consequence- to-life Category
	(a) _	Heavily Used Buildings residential building, commercial office, store and shop, hotel, factory, school, power station, ambulance depot, market, hospital, polyclinic, clinic, welfare centre	
1	(b)	Others	
	_	cottage, licensed and squatter areas	
	_	bus shelter, railway platform and other sheltered public waiting area	1
	_	dangerous goods storage site (e.g. petrol stations)	
	_	road with very heavy vehicular or pedestrian traffic density	
	(a)	Lightly Used Buildings	
	_	indoor car park, building within barracks, abattoir, incinerator, indoor games' sport hall, sewage treatment plant, refuse transfer station, church, temple, monastery, civic centre, manned substation	
2	(b)	Others	
	_	major infrastructure facility (e.g. railway, tramway, flyover, subway, tunnel portal, service reservoir)	
	_	construction site (if future use not certain) <sup>3</sup>	
	_	road <sup>4</sup> with heavy vehicular or pedestrian traffic density	2
3	_	heavily used open space and public waiting area (e.g. heavily used playground, open car park, heavily used sitting out area, horticulture garden)	
	_	road with moderate vehicular or pedestrian traffic density	
4	_	lightly used open-air recreation area (e.g. district open space, lightly used playground, cemetery, columbarium	
4	_	non-dangerous goods storage site	
	_	road with low vehicular or pedestrian traffic density	3
5	_	remote area (e.g. country park, undeveloped green belt, abandoned quarry)	
	_	road with very low vehicular or pedestrian traffic density	
Note:		The consequence-to-life category refers to the situation where to located within the expected travel distance of landslide debris or the influence zone of a failure. Situations where the CTL category car are given in GEO TGN No.15 (GEO, 2007).	e expected crest

<sup>&</sup>lt;sup>3</sup> If the intended future use is known, the Facility Group should be based on the facility that corresponds to the intended future use of the site.

<sup>&</sup>lt;sup>4</sup> For footpaths alongside roads, it may be assumed that footpaths are within the same group as the adjoining roads, except for Expressway (EX), Urban Trunk Roads (UT) and Rural Trunk Road (RT). Footpaths alongside EX, UT and RT roads may be taken, by default, as a Group 5 facility, unless dictated otherwise by site-specific conditions.

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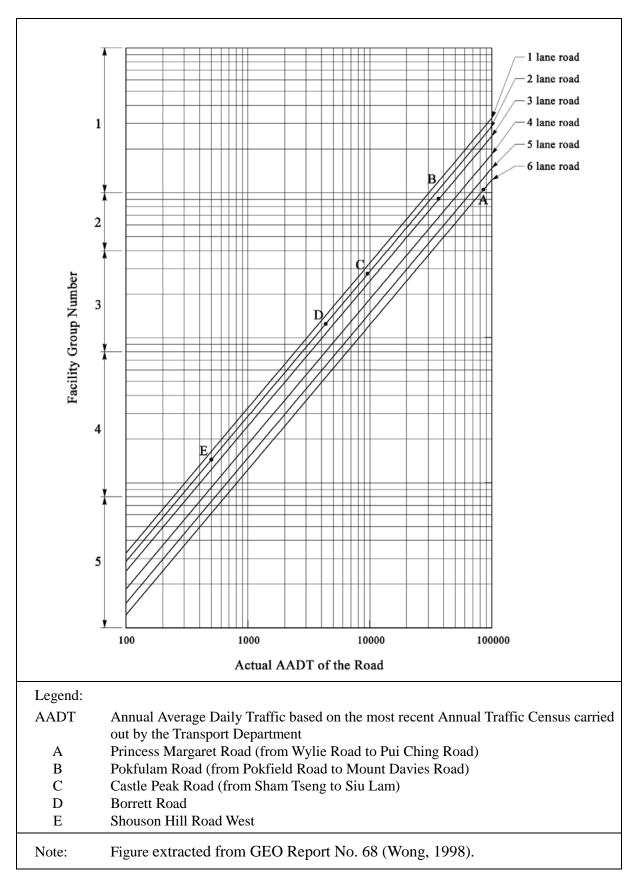


Figure 2.2 Relationship between Facility Groups, Actual AADT and Number of Traffic Lanes

- (c) Government rock cut slopes, fill slopes and retaining walls that were processed and accepted by GEO.
- (d) Private slopes and retaining walls that have been subjected to GEO Stage 2 studies after 2000, checked by GEO after 2000, checked and upgraded with robust technology, or subjected to DH orders.

Should severe signs of distress or instability be observed on the above slope features, safety nets (e.g. Engineer Inspections (EI), systematic landslide investigation programme, etc.) are available to initiate actions, e.g. urgent repairs and injection into the LPMitP.

Similar to NPCS, NPRS are essentially expert formulation systems (Wong, 2005), except for that on rock cut slopes which is an expert judgment system. In the latter system, the inspecting engineers need to exercise judgment in assessing the potential modes of instability and the corresponding probable scale of failures.

GEO has developed a database with standard templates for computation of ranking scores under NPRS. The database can be accessed and downloaded through the following link: (http://hkss.cedd.gov.hk/hkss/eng/nprs.aspx).

## 2.2 Selection of Cross-sections of Slope Features

In calculating the *TS*, the cross section corresponding to the worst-consequence (denoted as Section 1-1) should be considered. Where several facilities exist, either at the same section or at different sections across a slope feature, the potential consequence of failure in relation to each facility should be assessed to determine which facility and section would give rise to the most severe consequence. The section with the combination of crest and toe facilities which gives the highest *CS* should be selected as the worst-consequence section.

If the cross section with the maximum feature height (denoted as Section 2-2) is not the worst-consequence section, and the feature height at Section 1-1 is less than 75% of the feature height at Section 2-2, then the *TS* corresponding to both sections (i.e. Sections 1-1 and 2-2) should be computed and the higher *TS* value is taken to be representative of the slope feature.

## 2.3 Composite Slope Features

For composite slope features, i.e. with more than one type of slope feature present, the criteria for computation of the appropriate *TS* are given in Figures 2.3 and 2.4.

A methodology to combine the *TS* as calculated by the individual NPRS is presented in Section 7.

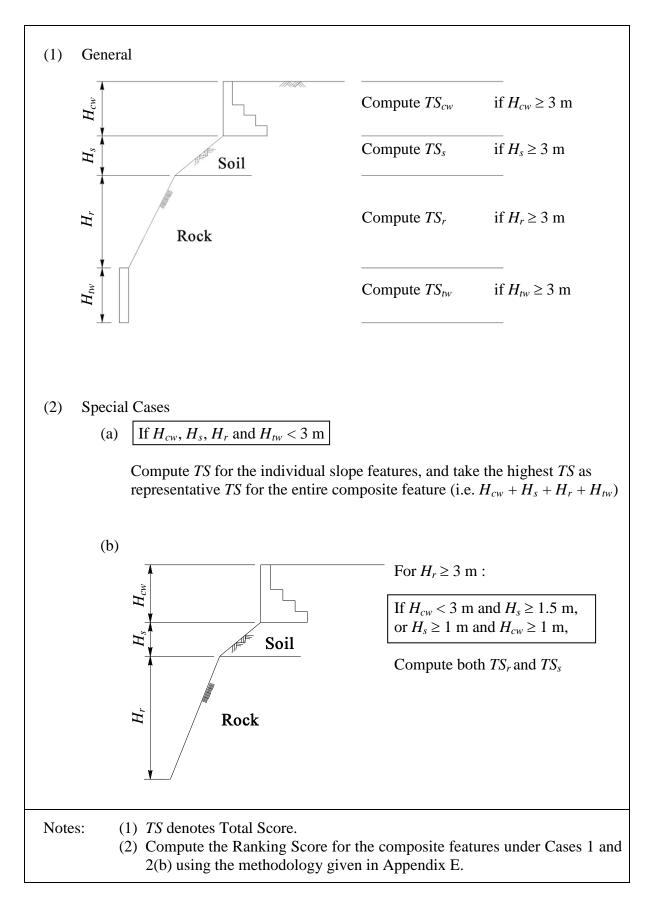
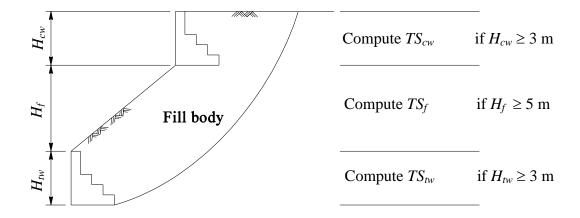


Figure 2.3 Computation of Ranking Scores for Composite Features Comprising Soil Cut Slope, Rock Cut Slope and Retaining Walls





## (2) Special Cases

(a) If 
$$H_{cw} \& H_{tw} < 3 \text{ m}$$
, and  $H_f < 5 \text{ m}$ , and if  $H_f + H_{cw} \ge 5 \text{ m}$ 

Compute  $TS_f$  and  $TS_{cw}$  and take the higher TS as the representative score for the entire composite feature (i.e.  $H_{cw} + H_f + H_{tw}$ )

(b) If 
$$H_{cw} \& H_{tw} < 3 \text{ m}$$
, and  $H_f < 5 \text{ m}$ , and if  $H_f + H_{tw} \ge 5 \text{ m}$ 

Compute  $TS_f$  and  $TS_{tw}$  and take the higher TS as the representative score for the entire composite feature (i.e.  $H_{cw} + H_f + H_{tw}$ )

Notes:

- (1) TS denotes Total Score.
- (2) Compute the Ranking Scores for the composite features under Case 1 using the methodology given in Appendix E.

Figure 2.4 Computation of Ranking Scores for Composite Features Comprising Fill Slope and Retaining Walls

#### 2.4 A Stack of Slope Features

The overall stability of a stack of slope features that are close to each other vertically may be more critical than the individual slope feature, and is related to the proximity of the slope features relative to one another as well as the failure mechanisms. The influence of the lower slope feature on the upper slope feature has been assessed by the past landslide records.

Based on past landslide records, it was established that the back scarp of a typical slope failure in Hong Kong would generally extend beyond the slope crest to a horizontal distance of less than 0.4 times the feature height (GEO, 2007). Figure 2.5 addresses the TS calculation for slope features close to each other vertically. The separation limits  $L_{AB}$  and  $L_{BC}$  shown in Figure 2.5 are for guidance only. Depending on the actual site conditions, possible nature of instability and interaction between the slope features, some slope features may have to be assessed as a stack even when the crest to toe distance is wider than the separation limits. The guidance given in Figure 2.5 is applicable to a stack of slope features consisting of slope features of the same type, or cut slopes and retaining walls, or fill slopes and retaining walls. For multiple retaining walls in terraced ground, reference should be made to the guidance on multiple walls given in Appendix D.

#### 2.5 Slope Features Requiring Immediate Action

Where there are significant signs of distress, or visual or documented evidence of continuous hazardous movement of slope features, or boulders or rock fragments, immediate follow-up action is recommended to be taken to remove or reduce the risk.

## 3 NPRS for Soil Cut Slopes

#### 3.1 The System

The system considers sliding and washout failures of soil cut slopes and computes a (TS) based on the likelihood of failure (IS) and the consequence of failure (CS), i.e.

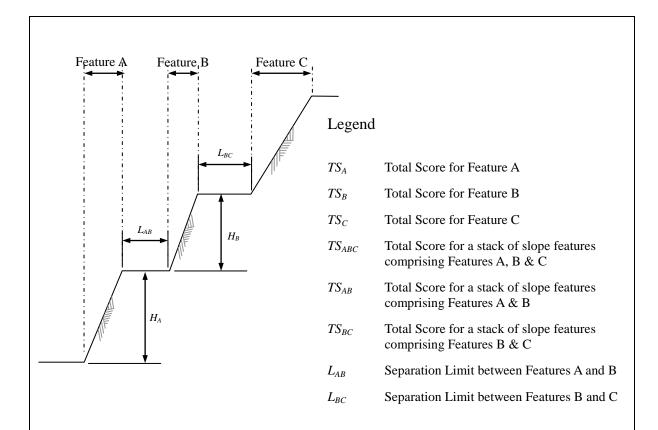
$$TS = IS \times CS$$

Details of the system and the guidelines, together with sample data collection sheets and a worked example, are presented in Appendix A.

#### 3.2 Instability Score

The IS comprises two components, which account for the Instability Potential (IP) and Actual Performance (AP) of the slope, i.e.

$$IS = IP \times AP$$



- 1. For computing *TS* for the lowest slope feature:
  - (a) If  $L_{AB} \le 0.4$   $H_A$  and  $L_{BC} \le 0.4$  ( $H_A + H_B$ ), consider a stack of features comprising Features A, B & C.

If 
$$TS_{ABC} > TS_A$$
, then  $TS_A = TS_{ABC}$ 

(b) If  $L_{AB} \le 0.4$   $H_A$  and  $L_{BC} > 0.4$   $(H_A + H_B)$ , consider a stack of slope features comprising Features A & B.

If 
$$TS_{AB} > TS_A$$
, then  $TS_A = TS_{AB}$ 

- 2. For computing TS for the middle slope feature:
  - (a) If  $L_{BC} \le 0.4 H_B$ , consider a stack of slope features comprising Features B & C.

If 
$$TS_{BC} > TS_B$$
, then  $TS_B = TS_{BC}$ 

3. TS for the uppermost slope feature remains unchanged

Note: TS denotes Total Score.

Figure 2.5 Computation of Total Score for a Stack of Slope Features

The IP is reflected by the age of the slope, level of geotechnical engineering input, slope geometry, provision of surface protection and surface drainage measures, and site characteristics, i.e. factors AI to AS in the equation below. The AP is manifested as signs of distress where present and records of instability after the slope has been formed or treated to its present configuration, i.e. factors BI and B2.

$$IS = A1 \times A2 \times A3 \times A4 \times A5 \times B1 \times B2...$$
 (3.1)

where A1 accounts for the age of slope since formation or treatment

A2 accounts for the level of geotechnical engineering input

A3 accounts for the slope geometry

A4 accounts for the adequacy of surface protection and surface drainage measures

A5 accounts for the site characteristics in respect of hydrogeological and geological settings

B1 accounts for signs of distress

B2 accounts for instability since slope formation or treatment

The weighting of individual factors in *IS* ranges between 1 and a value of less than or equal to 10, depending on their significance.

## 3.3 Consequence Score

The CS, which reflects the likely consequence of failure, is computed by the following equation:

$$CS = (C1 \times C2 + D1 \times D2) \times H$$
 .....(3.2)

where

C1 accounts for the type of crest facility

C2 accounts for the vulnerability of the crest facility (see Table 3.1)

D1 accounts for the type of toe facility

D2 accounts for the vulnerability of the toe facility (see Table 3.2)

*H* represents the feature height

The vulnerability factors given in Tables 3.1 and 3.2, where reflect the chance of fatality given the landslide, account for the height of the slope and the nature of the affected facilities together with their proximity to the slope.

## 4 NPRS for Rock Cut Slopes

## 4.1 The System

The system considers potential ravelling, toppling, wedge and planar failures of rock cut slopes and computes a *TS* based on the likelihood of failure (*IS*) and the consequence of failure (*CS*), i.e.

Details of the system and the guidelines, together with sample data collection sheets and a worked example, are presented in Appendix B.

Table 3.1 Vulnerability Factors for Crest Facilities Involving Soil Cut Slopes, Rock Cut Slopes and Retaining Walls

## (a) Vulnerability Factor (C2) for Crest Facility being Buildings

Feature	Distance from Crest, D (m)					
Height, $H(m)$	10 > D ≥ 6	6 > D ≥ 3	D < 3			
H < 5	0	0.0000125	0.0003			
5 ≤ <i>H</i> < 10	0	0.0000625	0.0015			
$10 \le H < 15$	0	0.00025	0.006			
$15 \le H < 20$	0.0002	0.003	0.02			
<i>H</i> ≥ 20	0.0005	0.01	0.05			

## (b) Vulnerability Factor (C2) for Crest Facility other than Buildings

Feature	Distance from Crest, D (m)					
Height, $H(m)$	10 > D ≥ 6	6 > D ≥ 3	D < 3			
H < 5	0	0.00025	0.0075			
5 ≤ <i>H</i> < 10	0	0.00125	0.0375			
$10 \le H < 15$	0	0.005	0.15			
$15 \le H < 20$	0.002	0.04	0.4			
<i>H</i> ≥ 20	0.002	0.074	0.54			

Notes:

- (1) Refer to Figure 2.1 for definition of feature geometry H and D.
- (2) For  $D \ge 10$  m, accord C2 = 0 for all feature heights.

Table 3.2 Vulnerability Factors for Toe Facilities Involving Soil Cut Slopes, Rock Cut Slopes and Retaining Walls

## (a) Vulnerability Factor (D2) for Toe Facility being Buildings

Feature	Shadow Angle, $\omega$ (degree)								
Height, H (m)	ω>50	50≥ ω>45	45 ≥ ω> 40	40≥ ω> 35	35 ≥ ω> 30	30≥ ω> 25	25 ≥ ω> 20		
H < 5	0.0225	0.0225	0.0155	0.005	0.001	0.0001	0		
5 ≤ <i>H</i> < 10	0.1125	0.1125	0.0775	0.025	0.005	0.0005	0		
$10 \le H < 15$	0.45	0.45	0.31	0.10	0.02	0.002	0		
$15 \le H < 20$	0.95	0.92	0.70	0.35	0.11	0.02	0		
<i>H</i> ≥ 20	0.95	0.95	0.86	0.59	0.26	0.075	0.013		

## (b) Vulnerability Factor (D2) for Toe Facility other than Buildings

Feature	Shadow Angle, $\omega$ (degree)								
Height, H (m)	ω>50	50≥ ω>45	45 ≥ ω> 40	40≥ ω> 35	35 ≥ ω> 30	30≥ ω> 25	25 ≥ ω> 20		
H < 5	0.03	0.03	0.026	0.016	0.006	0.00075	0		
5 ≤ <i>H</i> < 10	0.150	0.150	0.130	0.08	0.030	0.00375	0		
$10 \le H < 15$	0.60	0.60	0.52	0.32	0.12	0.015	0		
$15 \le H < 20$	0.95	0.92	0.92	0.70	0.49	0.08	0		
<i>H</i> ≥ 20	0.95	0.95	0.95	0.86	0.59	0.25	0.03		

Notes:

- (1) Refer to Figure 2.1 for definition of feature geometry H and  $\omega$ .
- (2) For  $\omega \le 20^{\circ}$ , accord D2 = 0 for all feature heights.

## 4.2 Instability Score

The IS comprises two components, which account for the Instability Potential (IP) and Actual Performance (AP) of the slope, i.e.

$$IS = IP \times AP$$

The IP is reflected by the level of geotechnical engineering input, slope geometry,

mode and scale of instability, seepage and drainage conditions, i.e. factors AI to A4 in the equation below. Similar to soil cut slopes, the AP is manifested as signs of distress where present and records of instability after the slope feature has been formed or treated to its present configuration, i.e. factors BI and B2.

$$IS = A1 \times A2 \times A3 \times A4 \times B1 \times B2.$$
 (4.1)

where

A1 accounts for the level of geotechnical engineering input

A2 accounts for slope geometry

A3 accounts for mode and scale of instability

A4 accounts for seepage and drainage conditions

B1 accounts for signs of distress

B2 accounts for instability since formation or treatment

The potential mode and scale of instability of a rock cut slope should be evaluated based on the inspecting engineer's site observations and documentary records on site geology, rock mass conditions, geological setting, and any relevant geological features. Reference should also be made to the previous failure incidents that occurred on the rock cut slope.

The weighting of individual factors in *IS* ranges between 1 and a value of less than or equal to 10, depending on their significance.

## **4.3** Consequence Score

The *CS*, which reflects the likely consequence of failure is computed by the following equation:

$$CS = (C1 \times C2 + D1 \times D2) \times K$$
 (4.2)

where

C1 accounts for the type of crest facility

C2 accounts for the vulnerability of the crest facility (see Table 3.1)

D1 accounts for the type of toe facility

D2 accounts for the vulnerability of the toe facility (see Table 3.2)

*K* accounts for the probable scale of failure

The vulnerability factors given in Tables 3.1 and 3.2, where reflect the chance of fatality given the landslide, account for the height of the slope and the nature of the affected facilities together with their proximity to the slope. The weighting of K ranges between 1 and 5, depending on the scale of failure.

## **5** NPRS for Fill Slopes

## 5.1 The System

The system considers the following failure modes of fill slopes:

(a) sliding and minor washout: common slope failures which do

not involve the build-up of excess pore water pressure and influence from a large amount of external water. debris slides downslope and may involve disintegration of the soil mass, particle collision and minor erosion and washout action:

- (b) liquefaction: mobile failure involving the generation of high positive excess pore water pressures during shearing and hence a substantial reduction of the effective stress and the shearing resistance; and
- (c) major washout: mobile failure involving concentrated discharge of water (e.g. surface runoff from a road) resulting in scouring and erosion of the slope and the washing of debris downslope.

The system computes a TS based on the likelihood of the different failure modes (IS) and the consequence of different failure modes (CS), i.e.

$$TS = \sum_{i=1}^{3} IS_i \times CS_i \qquad (5.1)$$

where  $IS_1$  and  $CS_1$  account for sliding and minor washout failure

 $IS_2$  and  $CS_2$  account for liquefaction failure

 $IS_3$  and  $CS_3$  account for major washout failure

Details of the system and the guidelines, together with sample data collection sheets and a worked example, are presented in Appendix C.

#### 5.2 Instability Score

The IS comprises two components, which account for the Instability Potential (IP) and Actual Performance (AP) of the slope, i.e.

$$IS = IP \times AP$$

The *IP* is reflected by the level of geotechnical engineering input and potential of various modes of failure to occur. The AP is manifested as signs of distress where present and records of instability after the slope has been formed or treated to its present configuration.

$$IS_1 = A1 \times A2 \times B1 \times B2...$$
 (5.2a)

$$IS_2 = A1 \times A3 \times B1 \times B2.$$
 (5.2b)

$$IS_3 = A1 \times A4 \times B1 \times B2.$$
 (5.2c)

1, 2 and 3 correspond to "sliding and minor washout failure", "liquefaction where failure" and "major washout failure" respectively

> accounts for the level of geotechnical engineering input A1

A2 accounts for factors affecting sliding and minor washout failure

A3 accounts for factors affecting liquefaction failure

A4 accounts for factors affecting major washout failure

B1 accounts for signs of distress

B2 accounts for instability since formation or treatment

The weighting of individual factors in *IS* ranges between 0.05 and 32, depending on their significance.

#### **5.3** Consequence Score

The CS, which reflects the likely consequence of different failure modes, is computed by the following equations:

$$CS_i = (C1 \times C2_i + D1 \times D2_i) \times H.$$
 (5.3)

where

*i* 1, 2 and 3 correspond to "sliding and minor washout failure", "liquefaction failure" and "major washout failure" respectively

C1 accounts for the type of crest facility

C2 accounts for the vulnerability of the crest facility (see Table 5.1)

D1 accounts for the type of toe facility

D2 accounts for the vulnerability of the toe facility (see Table 5.2)

*H* represents the feature height

The vulnerability factors given in Tables 5.1 and 5.2, where reflect the chance of fatality given the landslide, account for the height of the slope and the nature of the affected facilities together with their proximity to the slope.

## **6 NPRS for Retaining Walls**

#### **6.1** The System

The system considers partial and complete failure of retaining walls and computes a TS based on the likelihood of failure (IS) and the consequence of failure (CS), i.e.

$$TS = IS \times CS$$

Details of the system and the guidelines, together with sample data collection sheets and a worked example, are presented in Appendix D.

## **6.2 Instability Score**

The IS comprises two components, which account for the Instability Potential (IP) and Actual Performance (AP) of the wall, i.e.

$$IS = IP \times AP$$

**Table 5.1 Vulnerability Factors for Crest Facilities Involving Fill Slopes** 

## (a) Vulnerability Factor (C2) for Crest Facility being Buildings

Eastuma Haisaht	H (m)	Distance from Crest, D (m)					
Feature Height, H (m)		$10 > D \ge 6$	$6 > D \ge 3$	D < 3			
TT	$V_1=V_2$	0	0.0000125	0.0003			
H < 5	$V_3$	0	0.00023	0.0023			
5 × 11 × 10	$V_1=V_2$	0	0.0000625	0.0015			
$5 \le H < 10$	$V_3$	0	0.00115	0.0115			
10 . 77 . 17	$V_1=V_2$	0	0.00025	0.006			
$10 \le H < 15$	$V_3$	0	0.00715	0.0375			
$15 \le H < 20$	$V_1=V_2$	0.0002	0.003	0.02			
$13 \le H < 20$	$V_3$	0.008	0.0285	0.101			
11 > 20	$V_1=V_2$	0.0005	0.01	0.05			
$H \ge 20$	$V_3$	0.015	0.045	0.15			

## (b) Vulnerability Factor (C2) for Crest Facility other than Buildings

Feature Height, <i>H</i> (m)		Distance from Crest, $D$ (m)				
reature neight	, <i>H</i> (III)	$10 > D \ge 6$	$6 > D \ge 3$	D < 3		
H < 5	$V_1=V_2$	0	0.00025	0.0075		
H < 3	$V_3$	0	0.0022	0.011		
5 ≤ <i>H</i> < 10	$V_1=V_2$	0	0.00125	0.0375		
3 ≤ H < 10	$V_3$	0	0.011	0.055		
$10 \le H < 15$	$V_1=V_2$	0	0.005	0.15		
10 ≤ H < 13	$V_3$	0	0.043	0.18		
$15 \le H < 20$	$V_1=V_2$	0.002	0.04	0.4		
$13 \le H < 20$	$V_3$	0.004	0.092	0.2825		
<i>H</i> ≥ 20	$V_1=V_2$	0.002	0.074	0.54		
<i>H</i> ≥ 20	$V_3$	0.006	0.12	0.315		

Notes:

- (1) Refer to Figure 2.1 for definition of slope geometry H and D.
- (2)  $V_1$  = Vulnerability factor for sliding and minor washout failure

 $V_2$  = Vulnerability factor for liquefaction failure

 $V_3$  = Vulnerability factor for major washout failure.

(3) For  $D \ge 10$  m, accord C2 = 0 for all feature heights.

**Table 5.2 Vulnerability Factors for Toe Facilities Involving Fill Slopes** 

		(a	) Vulnerat	oility Facto	or (D2) for	Toe Facil	ity being H	Buildings				
Feature Height, H (m)			Shadow Angle, $\omega$ (degree)									
		ω>50	50≥ω>45	45≥ω>40	40≥ω>35	35≥ω>30	30≥ω>25	25≥ω>20	20≥ω>15	15≥ω>10		
	$V_I$	0.0225	0.0225	0.0155	0.005	0.001	0.0001	0	0	0		
H < 5	$V_2$	0.0225	0.0225	0.0225	0.0155	0.005	0.001	0.0001	0	0		
	$V_3$	0.010	0.008	0.004	0.002	0.0005	0.00008	0.000005	0	0		
	$V_I$	0.1125	0.1125	0.0775	0.025	0.005	0.0005	0	0	0		
$5 \le H < 10$	$V_2$	0.1125	0.1125	0.1125	0.0775	0.025	0.005	0.0005	0	0		
	$V_3$	0.05	0.04	0.02	0.01	0.0025	0.0004	0.000025	0	0		
	$V_I$	0.45	0.45	0.31	0.10	0.02	0.002	0	0	0		
$10 \le H < 15$	$V_2$	0.45	0.45	0.45	0.31	0.10	0.02	0.002	0	0		
	$V_3$	0.25	0.24	0.18	0.10	0.0425	0.0104	0.001525	0	0		
	$V_I$	0.95	0.92	0.70	0.35	0.11	0.02	0	0	0		
$15 \le H < 20$	$V_2$	0.95	0.95	0.95	0.8	0.48	0.18	0.045	0.005	0		
	$V_3$	0.60	0.60	0.56	0.45	0.29	0.135	0.0435	0.0076	0		
	$V_I$	0.95	0.95	0.86	0.59	0.26	0.075	0.013	0	0		
$H \ge 20$	$V_2$	0.95	0.95	0.95	0.95	0.87	0.63	0.34	0.12	0.015		
	$V_3$	0.80	0.80	0.80	0.72	0.50	0.25	0.084	0.015	0.001		

(b) Vulnerability Factor (D2) for Toe Facility other than Buildings

		` ′	<u> </u>	` `		<u> </u>					
Feature Height, H (m)		Shadow Angle, $\omega$ (degree)									
		ω>50	50≥ω>45	45≥ω>40	40≥ω>35	35≥ω>30	30≥ω>25	25≥ω>20	20≥ω>15	15≥ω>10	
\ <u></u>	$V_I$	0.03	0.03	0.026	0.016	0.006	0.00075	0	0	0	
H < 5	$V_2$	0.03	0.03	0.03	0.026	0.016	0.006	0.00075	0	0	
	$V_3$	0.040	0.036	0.025	0.013	0.004	0.001	0.0001	0	0	
	$V_I$	0.150	0.150	0.130	0.08	0.030	0.00375	0	0	0	
$5 \le H < 10$	$V_2$	0.15	0.15	0.15	0.13	0.08	0.03	0.00375	0	0	
	$V_3$	0.20	0.18	0.125	0.0625	0.02	0.005	0.0005	0	0	
	$V_I$	0.60	0.60	0.52	0.32	0.12	0.015	0	0	0	
$10 \le H < 15$	$V_2$	0.6	0.60	0.6	0.52	0.32	0.12	0.015	0	0	
	$V_3$	0.60	0.58	0.435	0.315	0.145	0.05	0.0105	0	0	
	$V_I$	0.95	0.92	0.92	0.70	0.49	0.08	0	0	0	
$15 \le H < 20$	$V_2$	0.95	0.95	0.95	0.95	0.80	0.50	0.20	0.02	0	
	$V_3$	0.875	0.875	0.835	0.725	0.530	0.285	0.1	0.0235	0	
<i>H</i> ≥ 20	$V_I$	0.95	0.95	0.95	0.86	0.59	0.25	0.03	0	0	
	$V_2$	0.95	0.95	0.95	0.95	0.95	0.8	0.50	0.20	0.02	
	$V_3$	0.95	0.95	0.95	0.95	0.81	0.48	0.18	0.045	0.005	

Notes:

- (1) Refer to Figure 2.1 for definition of slope geometry H and  $\omega$ .
- (2)  $V_1 = \text{Vulnerability factor for sliding and minor washout failure}$ 
  - $V_2$  = Vulnerability factor for liquefaction failure
  - $V_3$  = Vulnerability factor for major washout failure.
- (3) For  $\omega \le 10^{\circ}$ , accord D2 = 0 for all feature heights.

The IP is reflected by the level of geotechnical engineering input, wall slenderness, wall type, surface protection and surface drainage measures, seepage conditions and presence of leaky water-carrying services, i.e. factors AI to A5 in the equation below. The AP is manifested as signs of distress where present and records of instability after the retaining wall has been formed or treated to its present configuration, i.e. factors BI and B2.

$$IS = A1 \times A2 \times A3 \times A4 \times A5 \times B1 \times B2...$$
 (6.1)

where A1 accounts for the level of geotechnical engineering input

A2 accounts for wall slenderness ratio

A3 accounts for wall type

A4 accounts for adequacy of surface protection and surface drainage measures

A5 accounts for seepage conditions and the presence of leaky water-carrying services

B1 accounts for signs of distress

B2 accounts for instability since formation or treatment

The weighting of individual factors in *IS* ranges between 1 and a value of less than or equal to 10, depending on their significance.

## **6.3** Consequence Score

The CS, which reflects the likely consequence of failure, is computed by the following equation:

$$CS = (C1 \times C2 + D1 \times D2) \times H$$
 (6.2)

where *C1* accounts for the type of crest facility

C2 accounts for the vulnerability of the crest facility (see Table 3.1)

D1 accounts for the type of toe facility

D2 accounts for the vulnerability of the toe facility (see Table 3.2)

*H* represents the feature height

The vulnerability factors given in Tables 3.1 and 3.2, where reflect the chance of fatality given the landslide, account for the height of the wall and the nature of the affected facilities together with their proximity to the wall.

## 7 Combined Ranking

A method which ranks all types of slope features in terms of the relative risk of each slope feature has been developed. Using this method, a "Ranking Score" (RS) is calculated for each slope feature based on its "Total Score" (TS) in the respective NPRS. Details of the derivation of the RS are given in Appendix E.

For composite features, except the special cases illustrated in Figures 2.3 and 2.4, the individual RS for each of the feature types are summed up to obtain the RS for the slope feature. A worked example on the computation of RS for a composite feature is also

presented in Appendix E.

The *RS* is unique for each slope feature and can be used for priority ranking purposes under the post-2010 LPMitP. It can also be used by the Slope Maintenance Departments in the implementation of the post-2010 Preventive Maintenance Works.

#### 8 References

- GEO (2007). GEO Technical Guidance Note No. 15 Guidelines for Classification of Consequence-to-life Category for Slope Features. Geotechnical Engineering Office, Hong Kong, 14 p.
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# Appendix A

Details of NPRS for Soil Cut Slopes

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## **A.1** Total Score (TS) Computation Sheets for Soil Cut Slopes

FEA	ΓURE NO.	SECTION:	0		Severe Consequence) mum Feature Height)
(A)	INSTABILITY POTENTIAL (IP)				
(A1)	Year of Formation/Treatment (Y)				
	(i) <i>Y</i> ≤ 1980			<u>A1</u> 6	
	<ul><li>(ii) 1980 &lt; Y ≤ 1990</li></ul>			4	
	(iii) 1990 < <i>Y</i> ≤ 1995			2	
	(iv) $Y > 1995$			1	A1
	For soil cut slopes excluded from ranking (see Not	e 8), denote $AI = 0$	)		
(A2)	Level of Geotechnical Engineering Input				
				<u>A2</u>	
	(i) Slopes with none or little geotechnical engine	ering input		8	
	(ii) Slopes with indication of some geotechnical e			6	
	(iii) Slopes with indication of substantial geotechn	nical engineering in	put	2	A2
	(iv) Slopes checked and accepted by GEO			1	
(A3)	Geometry (refer to Figure A1)				
	(i) Soil Slope Height, $H_s$ m $(x)$	Feature Height, $H = H_s + H_r + H_c$		m	
	(ii) Rock Slope Height, $H_r$ m (xi)	$H_w = H_{cw} + H_{tw}$		m	
	(iii) Crest Wall Height, $H_{cw}$ m (xii)	$H_c = H_s + H_r$		m	
	(iv) Toe Wall Height, $H_{tw}$ m (xiii	$H_o = H_s + H_{cw} $	$+H_{r}$ ') $^{*}$	m	$*H_r'$ = rock slope portion where a realistic slip surface daylights
	(v) Upslope Angle, $\beta$	Effective Height, $T_e = H_o (1 + 0.35 \tan \rho)$	c	m	(see Note 14)
	(vi) Surcharge above the Slope		·		
	(vii) Soil Slope Angle, $\theta_s$				
	(viii) Average Slope Angle, $\theta$				
	(ix) Downslope Gradient, $\alpha$				

Geometry Classification (refer to Figure A2)       A3         (i) SI       8         (ii) S2       4         (iii) S3       2         (iv) S4       1						
Drainage						
Soil slope or crest area substantially unprotected	Soil slope or crest area partially protected	Soil slope or crest area substantially protected				
8	4	2				
4	2	1.5				
2	1.5	1	A4			
(A5) <u>Site Characteristics</u>						
tings	nt Moderate	Minor/None				
10	8	5				
8	3	2	A5			
5	2	1				
(B) ACTUAL PERFORMANCE (AP)						
)		## 10 4 1	B1			
	Drainage  Soil slope or crest area substantially unprotected  8  4  2  Significant 10  8  5	Soil slope or crest area substantially unprotected  8	Soil slope or crest area substantially unprotected   Soil slope or crest area substantially unprotected   Soil slope or crest area substantially protected   Soil slope or crest area substantially protected			

(B2)	Insta	ability after Slope Formation/Treatment	<u>B2</u>		
	(i)	Massive failures (> 500 m <sup>3</sup> )			
	(ii)	Major or repeated minor failures or records of previous severe signs of distress			
	(iii)	Minor failure or records of previous moderate signs			
	(iv)	No failure or records of previous minor signs of dis-	tress 1	B2	
(C)	FAC	CILITIES ABOVE CREST OF FEATURE			
	(i)	Type of crest facility (for roads and footpaths, give also the name) (refer to Table 2.1 of the main text)		Facility Group 1 (a)	<i>C1</i> 9
	(ii)	Facility Group		1 (b) 2 (a) 2 (b)	3 2 1
	(iii)	Distance (D) from crest of feature to crest facility (refer to Figure 2.1 of the main text)	m	3	0.25
				5 C1	0.0002
	(iv)	Vulnerability Factor, C2 (refer to Table 3.1 of the main text)		C2	
( <b>D</b> )	FAC	CILITY AT TOE OF FEATURE			
	(i)	Type of toe facility (for roads and footpaths, give also the name) (refer to Table 2.1 of the main text)		Facility Group 1 (a)	9
	(ii)	Facility Group		1 (b) 2 (a) 2 (b)	3 2 1
	(iii)	Distance ( <i>L</i> ) from toe of feature to toe facility (refer to Figure 2.1 of the main text)	m	3 4 5	0.25 0.002 0.0002
	(iv)	Shadow angle (a) from crest of feature to toe facility (refer to Figure 2.1 of the main text)	0	D1	
	(v)	Vulnerability Factor, D2 (refer to Table 3.2 of the main text)		D2	

CALCULATED SCORES	
INSTABILITY SCORE (IS)	
$IS = A1 \times A2 \times A3 \times A4 \times A5 \times B1 \times B2$	IS
CONSEQUENCE SCORE (CS)	
$CS = [C1 \times C2 + D1 \times D2] \times H$	CS
TOTAL SCORE (TS)	
$TS = IS \times CS$	TS

#### A.2 Guidelines on Data Collection and Score Computation for Soil Cut Slopes

#### General

- (1) For composite features, i.e. with more than one type of slope feature, the criteria for computation of the Total Score (*TS*) are presented in Figure 2.3 of the main text.
- (2) If H of Section  $1-1 \ge 75\%$  of H of Section 2-2, consider Section 1-1 (i.e. in terms of most severe consequence) in calculating the scores. Otherwise, both Sections 1-1 and 2-2 (in terms of maximum feature height, H) shall be considered.
- (3) Geometric parameters of the feature (e.g.  $H_s$ ,  $H_r$ ,  $H_{cw}$ ,  $H_{tw}$ ,  $\beta$ ,  $\theta_s$ ,  $\theta$  and  $\alpha$ ) (see Figure A1) may be obtained from survey plans and site measurements.
- (4) Detailed physical inspection on the features should be carried out using all available access/route.
- (5) Unless stated otherwise, "distance" refers to horizontal distance and "height" refers to vertical height.
- (6) Details of field mapping and site observation should be recorded using data collection sheets. Sample data collection sheets for soil cut slopes are appended for reference. Inspecting engineers may modify the sheets to suit their specific use. Provide photographic records of the overview of the features and facilities affected. The photographic records shall also include details of site observations to substantiate the factors adopted in the calculation.

#### Factor A1

- (7) Years of formation/treatment refers to the year that the formation or substantial modification works completed on the subject slope. Substantial modification works refer to the engineering works to bring substandard slopes to the safety standards at that time.
- (8) Slopes that were formed/treated in or after year 2000 or treated with robust technology (i.e. installed with structural support, e.g. soil nails), and processed and accepted by GEO, will not be ranked. Denote these features with AI = 0. Data on these slopes should still be collected.

#### Factor A2

- (9) The level of geotechnical engineering input should be inferred from databases, files and documentary records kept by GEO and other relevant government departments and organizations, or interpretation of aerial photographs if necessary.
- (10) Slopes with none or little geotechnical engineering input, e.g.
  - pre-1978 slopes

- post-1978 slopes formed by unauthorized works
- post-1978 slopes falling outside any engineering project boundary
- (11) Slopes with indication of some geotechnical engineering input, e.g.
  - post-1978 slopes without GEO checking records but falling within the boundary of engineering projects
  - slopes assessed as being upto the required safety standard without site-specific ground investigation and laboratory testing
- (12) Slopes with indication of substantial geotechnical engineering input, e.g.
  - slopes checked by GEO but with outstanding comments
- (13) Slopes checked and accepted by GEO, e.g.
  - slopes checked by GEO without outstanding comments
  - slopes designed by GEO

#### Factor A3

- (14) Definition of geometric parameters are given in Figure A1.  $H_o$  is the difference in elevations between the crest of the feature and the lowest daylighting point of realistic slip surfaces. In the case where the lowest daylighting point is at the toe of the soil portion of the slope,  $H_o$  should be calculated as  $H_s + H_{cw}$ . Otherwise,  $H_o$  should be taken to include the portion of the rock slope  $(H_r)$  where a realistic failure surface can daylight. The definition of effective height,  $H_e$ , takes into account the equivalent surcharging effect due to the uphill slope and applied vertical loading. An assessment of the surcharge (s) above the slope crest may be made by reference to Table 16 of the second edition of Geoguide 1 (GEO, 1993).
- (15) The factor A3 involves combined consideration of the effective height,  $H_e$ , and average slope angle ( $\theta$ ) as defined in Figure A2.

#### Factor A4

- (16) Both hard cover and vegetation cover are considered as slope protection. As a general guideline, "substantially protected" refers to more than 75% area covered, "partially protected" refers to between 25% and 75% area protected and "substantially unprotected" refers to less than 25% area covered.
- (17) Crest area refers to the area within a horizontal distance of H/2 beyond the crest of the slope.
- (18) Where there is potential for ponding above the slope crest, the score for the next higher category in respect of slope protection should be adopted.
- (19) In assessing the adequacy of surface drainage provisions, the overall setting including the site topography, catchment area and environmental factors that are liable to give rise to convergent flow of surface water should be considered.

(20)The potential for convergent flow of surface water above crest and whether the slope is located on a drainage line or depression shall be determined from topographic plan and/or aerial photographs.

#### Factor A5

As a general guideline, adverse hydrogeological settings are as follows: (21)

Significant observable or recorded adverse groundwater conditions, e.g. high permanent groundwater over a significant area of the slope; complex groundwater conditions with a significant storm response or delayed response; seepage at or above mid-height of slope

Moderate seepage below mid-height of slope

Minor/None no signs of seepage

(22)As a general guideline, adverse geological features are as follows:

Significant sites with relict massive failures; observable or recorded adverse discontinuities (e.g. adversely oriented, persistent, clay- or silt-infilled discontinuities, pre-existing shear surfaces or zones, and well developed discontinuities that are slickensided or heavily coated with dark minerals or kaolinite)

Moderate observable or recorded adverse geological materials (e.g. significantly

kaolinised granite and volcanics, weathered dykes, and sedimentary

layers within volcanic formations)

Minor/None none of the above

#### Factors B1 and B2

- (23)Signs of distress are based on site observations, and relevant inspection and maintenance records kept by the maintenance departments.
- (24)Severe signs of distress refer to signs of slope movement, e.g. large tension cracks behind crest, significant distortion of channels and berms, severe cracking and bulging, subsidence of slope crest or slope surface. These tell-tale signs should be examined in a holistic manner to determine if they are indicative of slope movement. Where there are severe signs of distress or documented evidence of continuing hazardous movement, immediate action should be taken. Examples of severe signs of distress are attached in Appendix F of this report.
- (25)Moderate signs of distress refer to signs of extensive minor defects, e.g. cracking of slope cover and damaged channels.
- Judgment should be made in assessing whether cracked slope cover, damaged channels, (26)etc. are due to inadequate maintenance. If these are due to inadequate maintenance, they should not be regarded as signs of distress. In case of doubt, a conservative

assessment should be made.

(27) Instability after treatment accounts for landslide incidents that occurred after the slope was formed or substantially modified to its present configuration, and upgrading works have not been carried out on the slope subsequent to the incidents.

### Factors C and D

(28) Shadow angle ( $\omega$ ) as shown in Figure 2.1 of the main text should be determined by site measurements and/or from survey plans and sections.

### References

GEO (1993). *Guide to Retaining Wall Design (Geoguide 1), 2<sup>nd</sup> Edition.* Geotechnical Engineering Office, Hong Kong, 258 p.

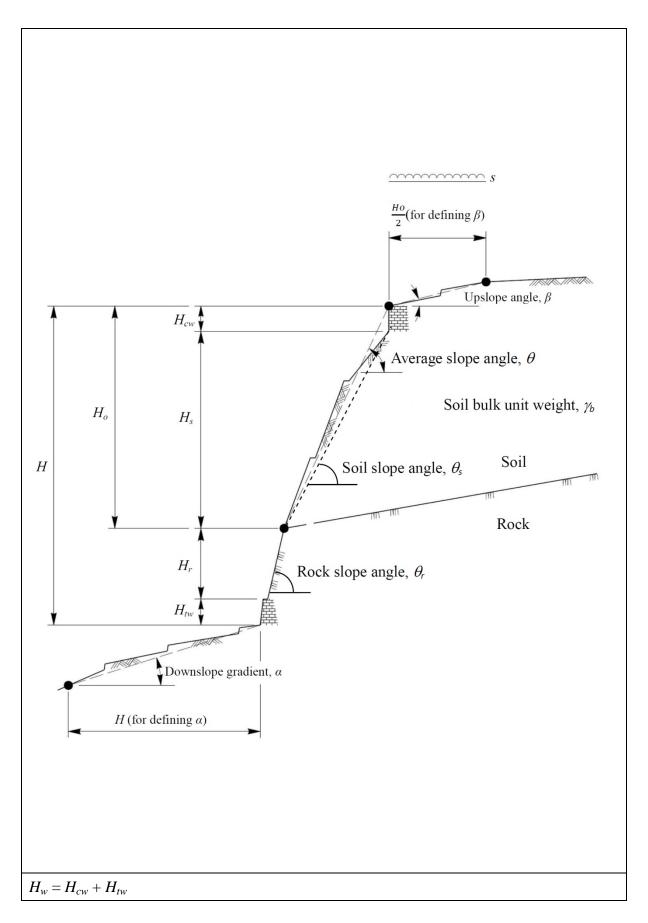


Figure A1 Geometry of Soil and Rock Cut Slopes

42

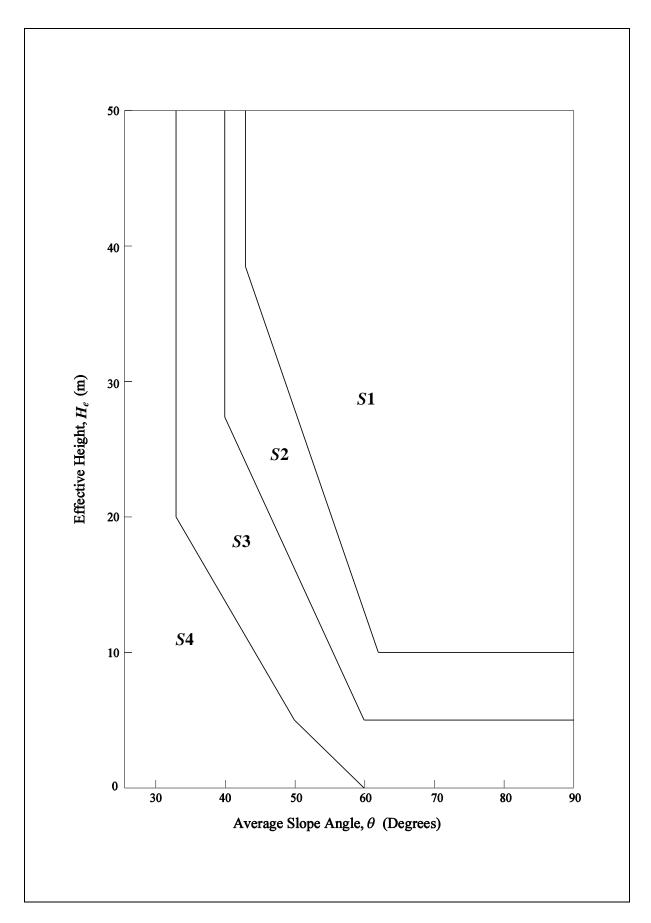


Figure A2 Geometry Classification for Soil Cut Slopes

# **A.3** Sample Data Collection Sheets for Soil Cut Slopes

FEATURE NO.						(Page 1 of )	
	D 1-1 (Most S	evere Conseque	ence)	O 2-2	(Maximum F		
Check if $H_1 \ge 75\% \times H_2$	$H_2$ . If yes, consid	er Section 1-1	only; If No,	consider both Section	ons 1-1 and 2-2	2	
Geometry (refer to Fig	gure A1)						
	Section 1-1	2-2			Section 1-1	2-2	
Soil Slope Height,		m	Feature Ho $H = H_s + H_s$	eight, $H_r + H_{cw} + H_{tw}$	m	m	
Rock Slope Height	, $H_{\rm r}$ m	m	$H_w = H_{cw}$ H	$+H_{tw}$	m	m	
Crest Wall Height, $H_{cw}$	m	m	$H_c = H_s +$	$H_r$	m	m	
Toe Wall Height, H	I <sub>tw</sub> m	m	$H_o = H_s +$	$H_{cw}\left(+H_{r}'\right)^{\#}$	m	m	
Upslope Angle, $\beta$	gle, $\beta$ $\beta$ $\beta$ $\beta$ $\beta$ $\beta$ $\beta$ $\beta$						
Surcharge above the Slope Crest, s	kPa	kPa	$H_r$ '		m	m	
			Effective H	leight, $H_e$			
Soil Slope Angle, &	9,	О	$H_e = H_o (1$	$+0.35 \tan \beta + \frac{s}{\gamma_b}$	m	m	
Average Slope Ang $\theta$	le, o	0		·			
Downslope Gradien $\alpha$	nt, o	0		where $\gamma_b = \text{soil bulk}$	unit weight	$\frac{kN}{m^3}$	
Do the dimensions of individual feature types satisfy the requirement of separate Total Score as shown in Figure 2.3 of the main text?  O Yes  No  No  If yes, number of data collection sheets required for this section:							
	- 1.0 II	yes, number of	uata coneci	non succis required	ioi uns secuoi	1.	
Affected Facilities (Re	efer to Figure 2.1 a	nd Table 2.1 of	the main te	xt)			
Section 1-1	Facility Type (for	r roads, please	give name)	Facility Group		oximity	
Toe					$L = \omega =$	m o	
Crest					D=	m	
Section 2-2	Facility Type (for	r roads, please	give name)	Facility Group	Pro	oximity	
Toe					$L = \omega =$	m o	
Crest					<i>D</i> =	m	

FEATURE NO.				(Page 2 of )
PLAN AND CROSS-SECTION	N			
SECTION: O 1-1	(Most Severe Consequen	ce)	0	2-2 (Maximum Feature Height)
Notes:  PLAN (1:1000)  1. Feature boundary (SIS) and revised feat 2. Section mark 3. Photograph location and direction 4. Signs of distress, if any 5. Signs of seepage, if any 6. Engineering measures (e.g. soil nails, sl	ture boundary (if applicable) 1 2	CROSS-SECTIONS  Fully dimensioned Engineering measures	(e.g. soil n	ails, shotcrete & buttress)

FEATURE NO.								(Page 3 of )
SLOPE CHARACTERISTICS			SITE O	BS	ERVATIONS/F	INDIN	GS	
Slope Protection	<ul> <li>Hard</li> <li>Bare:</li> <li>Other</li> <li>Based on t</li> <li>Subs</li> <li>Parti</li> <li>Subs</li> <li>Zone(s) of c</li> <li>Y</li> <li>If yes, m</li> </ul>	tationcoversurface_csthe above stantially ally protestantially depression depression ark the object.	ve, slope sur protected (> ected (25% - unprotected on or potentia	% (i % face 75% 75% (< 2	5) 5%) nding exist within ion or ponding zo	chunan	n) et area (within h	
Surface Drainage Provision	or inferr o Slope lo o Inadequ	red from ocated of ate surf	n topograph n a drainage ace drainag	nven	Type (e.g. U-charstep channel, downpipes or discovered by surface	et area cotos) ssion erosion	or erosion g	
Hydrogeological Settings  (Provide photographic records of signs of seepage and indicate location & extent on plan & cross-sections)	At or above Below mid-h	de follo age Loc mid-hei neight	ation				o Non of seepage ing/damp	Stain
Geological Features  (Provide photographic records of the site observations)	Presence of th  O No pote  O Possible  O Shear su  O Clay or  O Slickens  O Disconti	ne follow ntial ad- e relict f urfaces/z silt fille sided dis- inuities antly ka	ving based overse geologialure (concarone discontinuitie heavily coaroninised grant continuitie discontinuitie	on sigical average autices	ite observations I features observ shaped profile) s with dark miners or volcanics layers within vol	ved or re	ecorded aolinite	(please tick):

FEATURE NO.	(Page 4 of )
SLOPE CHARACTERISTICS	SITE OBSERVATIONS/FINDINGS
	<ul> <li>No indication of any signs of distress</li> <li>Reported signs of distress in inspection or maintenance records</li> </ul>
Signs of Distress  (Provide photographic records of signs of distress and indicate location & extent on plan & cross-sections)	<ul> <li>Observed signs of distress (please tick)</li> <li>Large tension cracks behind crest (approx mm wide)</li> <li>Significant distortion/damage of channels and berms</li> <li>Severe cracking and bulging of hard surfacing</li> <li>Subsidence within crest area or on slope</li> <li>Extensive cracking of slope cover</li> <li>Isolated minor cracking of slope cover/isolated cracking of channels</li> <li>Others:</li> <li>Where severe signs of distress or hazardous movements are noted, appropriate follow-up action should be taken immediately.</li> <li>Judgment should be made in assessing whether cracked slope cover, damaged channels etc. are due to inadequate maintenance; if so, they should not be regarded as signs of distress.</li> </ul>
Instability after Slope Formation/Treatment  (Provide photographic records of the inferred failure scar and indicate location on plan & cross-sections)	<ul> <li>No indication of any failure occurred after formation or treatment</li> <li>Reported failure</li></ul>
OTHER OBSERVATIONS/F	REMARKS

INSPECTION DATE: / / (dd/mm/yyyy) BY:

FEATURE NO.	(Page 5 of )
PHOTOGRAPHIC RECORDS	
[Caption]	
PHOTOGRAPHIC RECORDS	
[Caption]	
Notes:	
(1) Indicate photograph vantage points on plan (2) Add more pages for additional photographic records/sketches	

# **A.4** Worked Example (Data Collection Sheets)

ECTION: $\checkmark$ neck if $H_1 \ge 75\% \times H_2$ .	•	evere Conseque	ence) O only; If No, consider both	2-2 (Maximum	•
eometry (refer to Figure		ici Section 1-1	only, if ivo, consider both	i Sections 1-1 and 2	-2
Soil Slope Height, $H_s$	Section 1-1  12 m	2-2 — m	Feature Height, $H = H_s + H_r + H_{cw} + H_t$	Section 1-1  12 m	2-2 — m
Rock Slope Height, $H_r$	0 m	_ m	$H_w = H_{cw} + H_{tw}$	0	— m
Crest Wall Height, $H_{cw}$	0 m	_ m	$H_c = H_s + H_r$	12 m	_ m
Toe Wall Height, $H_{tw}$	0 m	_ m	$H_o = H_s + H_{cw} \left( + H_r \right)^{\sharp}$	12 m	— m
Upslope Angle, $\beta$	20 °	0	$^{\#}$ $H_o$ should include the slope where a realistic		
Surcharge above the Slope Crest, <i>s</i>	0 kPa	— kPa	$H_r$ '	0 m	— m
Soil Slope Angle, $\theta_s$	60 °	0	Effective Height, $H_e$ $H_e = H_o (1 + 0.35 \tan \beta) + 0.35 \tan \beta$	$\frac{s}{\gamma_b}$ 13.5 m	— m
Average Slope Angle, $\theta$	<b>60</b> °				
Downslope Gradient, $\alpha$	<b>0</b> °	o	where $\gamma_b = soi$	l bulk unit weight	$20\frac{kN}{m^3}$

## Affected Facilities (refer to Figure 2.1 and Table 2.1 of the main text)

Yes

Section 1-1	Facility Type (for roads, please give name)	Facility Group		Proximity	
Toe	Road with heavy traffic density	2(b)	<i>L</i> = ω=	0 m 60 °	
Crest	Undeveloped green belt	5	D=	0	m
Section 2-2	Facility Type (for roads, please give name)	Facility Group		Proximity	
			L=	_	m
Toe	_	_	$\omega =$	_	o

If yes, number of data collection sheets required for this section:

## FEATURE NO. "Worked Example 1"

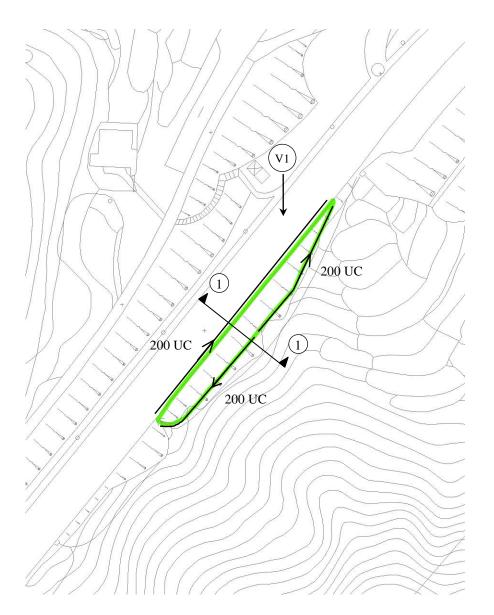
(Page 2 of 6)

#### PLAN AND CROSS-SECTION

**SECTION:** 

1-1 (Most Severe Consequence)

2-2 (Maximum Feature Height) 0



<u>Plan</u> (Not to scale)

- Feature boundary (SIS) and revised feature boundary (if applicable)
  Section mark
  Photograph location and direction
  Signs of distress, if any

- Signs of seepage, if any Engineering measures (e.g. soil nails, shotcrete & buttress)

#### CROSS-SECTIONS

- Fully dimensioned
   Engineering measures (e.g. soil nails, shotcrete & buttress)

# FEATURE NO. "Worked Example 1" (Page 3 of 6) PLAN AND CROSS-SECTION **SECTION:** 1-1 (Most Severe Consequence) 2-2 (Maximum Feature Height) Worked example 1 Undeveloped greenbelt Vegetated cover Shotcrete cover Road with heavy traffic density L = 0.5 m $\omega = 60^{\circ}$

Note: No reinforcement or structural support observed on site

200 UC

## **Section 1-1** (Not to scale)

- Feature boundary (SIS) and revised feature boundary (if applicable)
- Section mark

- Photograph location and direction Signs of distress, if any Signs of seepage, if any Engineering measures (e.g. soil nails, shotcrete & buttress)

#### **CROSS-SECTIONS**

- Engineering measures (e.g. soil nails, shotcrete & buttress)

FEATURE NO. "Worke	ed Example	e 1"					(Page 4 of 6)	
SLOPE CHARACTERISTICS			SITE OB	SERVATIONS/F	INDIN	GS		
Slope Protection	Surface cover with  Vegetation							
	Location	Size (mm)	Spacing (m)	Type (e.g. U-ch step channe downpipes or c	el,	Adequate Capacity (Y/N)	Remarks	
	Crest	200	_	U-channo	el	Y	Lined	
Surface Drainage Provision	Berm	_	-   -   -			_		
	On Slope	_	_					
Surrue Dimmige Trovision	Toe	200	_	U-channo	el	Y	Lined	
	<ul> <li>Potential surface runoff converge onto the crest area due to topo or inferred from topographic plan or aerial photos)</li> <li>Slope located on a drainage line/zone of depression</li> <li>Inadequate surface drainage evident by surface erosion or erosion</li> <li>Others observations/records:</li> </ul>							
Hydrogeological Settings	Signs of See		1 . 7	0	Yes	√ No	)	
	If Yes, prov			Condition of seepage				
(Provide photographic records of signs of seepage	See	page Locati	on	Copious	Trickl	ing/damp	Stain	
and indicate location &	At or above	mid-height	t					
extent on plan & cross-sections)	Below mid-	height						
	o Others	observation	ns/records:					
Geological Features  (Provide photographic records of the site observations)	<ul> <li>No pot</li> <li>Possible</li> <li>Shear set</li> <li>Clay or</li> <li>Slicker</li> <li>Discon</li> <li>Signifi</li> </ul>	Below mid-height  Others observations/records:  Presence of the following based on site observations & available records (please tick):  No potential adverse geological features observed or recorded  Possible relict failure (concave shaped profile)  Shear surfaces/zone  Clay or silt filled discontinuities  Slickensided discontinuities  Discontinuities heavily coated with dark minerals or kaolinite  Significantly kaolinised granite or volcanics						

SLOPE CHARACTERISTICS	SITE OBSERVATIONS/FINDINGS
<u> </u>	<ul> <li>✓ No indication of any signs of distress</li> <li>○ Reported signs of distress in inspection or maintenance records</li> </ul>
Signs of Distress  (Provide photographic records of signs of distress and indicate location & extent on plan & cross-sections)	<ul> <li>Observed signs of distress (please tick)</li> <li>Large tension cracks behind crest (approx mm wide)</li> <li>Significant distortion/damage of channels and berms</li> <li>Severe cracking and bulging of hard surfacing</li> <li>Subsidence inside crest area or on slope surface</li> <li>Extensive cracking of slope cover</li> <li>Isolated minor cracking of slope cover/Isolated cracking of channels</li> <li>Others:</li> <li>Where severe signs of distress or hazardous movement is noted, appropriate follow-up action should be taken immediately.</li> <li>Judgment should be made in assessing whether cracked slope cover, damaged channels etc. are due to inadequate maintenance, if so, they should not be regarded as signs of distress.</li> </ul>
Instability after Formation/Treatment	<ul> <li>No indication of any failure occurred after formation or treatment</li> <li>Reported failure Minor inferred past instability recorded in SIRST in 1999</li> </ul>
(Provide photographic records of the inferred failure scar and indicate location on plan & cross-sections)	O Possible failure scar observed at of the slope  Estimated failure volume = m <sup>3</sup> O Debris observed on site/Other observations:
OTHER OBSERVATIONS/R	EMARKS
development or mo	SIFT report, the slope was formed pre-1963. No record of any dification works carried out on the feature.  were recorded in SIRST in 1999.

# FEATURE NO. "Worked Example 1"

(Page 6 of 6)

PHOTOGRAPHIC RECORDS



V1 General View of the Feature

# Notes:

- (1)
- Indicate photograph vantage points on plan Add more pages for additional photographic records/sketches

# **A.5** Worked Example (TS Computation Sheets)

FEAT	TURE NO. "Worked Example 1"	SECTION:		t Severe Consequence) imum Feature Height)
(A)	INSTABILITY POTENTIAL (IP)			
(A1)	Year of Formation/Treatment (Y)			
			<u>A1</u>	
	(i) $Y \le 1980$		6	
	(ii) $1980 < Y \le 1990$		4	
	(iii) $1990 < Y \le 1995$		2	A1 6
	(iv) $Y > 1995$		1	, ii
	For soil cut slopes excluded from ranking (see Not	te 8), denote $A1 = 0$	)	
(A2)	Level of Geotechnical Engineering Input			
			<u>A2</u>	
	(i) Slopes with none or little geotechnical engine	-	8	
	(ii) Slopes with indication of some geotechnical e	engineering input	6	8
	(iii) Slopes with indication of substantial geotechr	nical engineering ir	iput 2	A2   6
	(iv) Slopes checked and accepted by GEO		1	
(A3)	Geometry (refer to Figure A1)			
	(i) Soil Slope Height, $H_s$ 12 m $(x)$	Feature Height, $H = H_s + H_r + H_{cv}$		
	(ii) Rock Slope Height, $H_r$ <b>0 m</b> (xi)	$H_w = H_{cw} + H_{tw}$	0 m	
	(iii) Crest Wall Height, $H_{cw}$ <b>0 m</b> (xii)	$H_c = H_s + H_r$	0 m	
	(iv) Toe Wall Height, $H_{tw}$ 0 m (xiiii	$H_o = H_s + H_{cw} (+$	12 m	* <i>H<sub>r</sub></i> ' = rock slope portion where a realistic slip surface daylights (see Note 14)
	(v) Upslope Angle, $\beta$ 20 °	Effective Height, $I_e = H_o (1 + 0.35 \tan \mu)$		(see Note 14)
	(vi) Surcharge above the Slope Crest, s 0 kPa		7.6	
	(vii) Soil Slope Angle, $\theta_s$ 60 °			
	(viii) Average Slope Angle, $\theta$ 60 °			
	(ix) Downslope Gradient, $\alpha$ 0 °			

Geometry Classification (refer to Fig	gure A2)		<u>A3</u>	
(i) <i>S1</i>	,		8	
(ii) S2			4	
(iii) <i>S3</i>			2	A3 4
(iv) <i>S4</i>			1	A3 4
(A4) Slope Protection and Surface	<u>Drainage</u>			
Slope Protection	Soil slope or	Soil slope or	Soil slope or	
Slope Protection	crest area	crest area	crest area	
Surface Drainage	substantially unprotected	partially protected	substantially protected	
Few or no channels, and potential for convergent flow of surface water above crest or located on a drainage line or depression	8	4	2	
Few or no channels	4	2	(1.5)	
Adequate channels	2	1.5	1	A4 1.5
Adverse hydrogeological Adverse geological feature	gical tings Significa	nt Moderate	Minor/None	
Significant	10	8	5	
Moderate	8	3	2	A5 <b>1</b>
Minor/None	5	2	1	
(B) ACTUAL PERFORMANCI	E (AP)			
(B1) Signs of Distress			n i	
(i) Severe	t)		<u>B1</u> 10	
(signs of slope movemen  (ii) Moderate			4	B1 1
(extensive minor defects)	)			
(iii) Minor/None (none or few isolated min	nor defects)		1	

(B2)	Insta				
	(i)	Massive failures (> 500 m <sup>3</sup> )	<u>B2</u> 10		
		Major or repeated minor failures or records of previous severe signs of distress	5		
	(iii)	Minor failure or records of previous moderate signs of	of distress 2		
	(iv)	No failure or records of previous minor signs of distr	ess 1	B2	2
(C)	FAC	CILITIES ABOVE CREST OF FEATURE			
	(i)	Type of crest facility (for roads and footpaths, give also the name) (refer to Table 2.1 of the main text)	Undeveloped green belt	Facility Group 1 (a)	<i>CI</i> 9
	(ii)	Facility Group	5	1 (b) 2 (a) 2 (b)	2
	(;;;)	Distance (D) from crest of feature to crest		3	0.25
	(111)	facility (refer to Figure 2.1 of the main text)	0 m	4	0.002
				5	0.0002
				C1	0.0002
	(iv)	Vulnerability Factor, C2 (refer to Table 3.1 of the main text)		C2	0.15
( <b>D</b> )	FAC	CILITY AT TOE OF FEATURE		1	
	(i)	Type of toe facility (for roads and footpaths, give also the name) (refer to Table 2.1 of the main text)	Road/footpath with heavy traffic density	Facility Group 1 (a)	<i>D1</i>
				1 (b)	3
	(ii)	Facility Group	2(b)	2 (a)	2
			, ,	2 (b)	1 0.25
	(iii)	Distance (L) from toe of feature to toe facility		3 4	0.25
		(refer to Figure 2.1 of the main text)	0.5 m	5	0.0002
	(iv)	Shadow angle ( $\omega$ ) from crest of feature to toe facility (refer to Figure 2.1 of the main text)	60°	DI	1
	(v)	Vulnerability Factor, D2 (refer to Table 3.2 of the main text)		D2	0.6

CALCULATED SCORES		
INSTABILITY SCORE (IS)		
$IS = A1 \times A2 \times A3 \times A4 \times A5 \times B1 \times B2$	IS	576
CONSEQUENCE SCORE (CS)		
$CS = [C1 \times C2 + D1 \times D2] \times H$	CS	7.20
TOTAL SCORE (TS)		
$TS = IS \times CS$	TS	4147.2

# Appendix B

Details of NPRS for Rock Cut Slopes

# Contents

		Page No.
Con	tents	59
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B.1	Total Score (TS) Computation Sheets for Rock Cut Slopes	61
B.2	Guidelines on Data Collection and Score Computation for Rock Cut Slopes	65
B.3	Sample Data Collection Sheets for Rock Cut Slopes	69
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# **List of Figure**

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# **B.1** Total Score (TS) Computation Sheets for Rock Cut Slopes

FEATURE NO.										
(refer to Figure B1)					(v)	Feature	Heigh	ht, H = 1	$H_r + H_s + H_s$	$H_{cw} + H_{tw}$
(i) Rock Slope Height,	$H_r = $			_m				= .		m
(ii) Soil Slope Height, H	$H_s = \underline{\hspace{1cm}}$			_m	(vi)	Rock S	lope A	ngle, $\theta_r =$		О
(iii) Crest Wall Height, H							_	gle, $\theta_s = 1$		
(iv) Toe Wall Height, $H_t$							Ι.	6 - 7 - 3		
(A) INSTABILITY P	OTENT	TAL (	<b>IP</b> )		I					
(A1) Level of Geotechn	nical Eng	ineerir	ng Input							
(i) Slopes with none or little geotechnical engineering input  (ii) Slopes with indication of some geotechnical engineering input  3 (iii) Slopes with indication of substantial geotechnical engineering input  1  For rock cut slopes excluded from ranking (see Note 7), denote $AI = 0$										
(A2) Geometry										
Rock Slope Angle $(\theta_r)$ Feature Height $(H)$	$\theta_r > 80^{\circ}$		$<\theta_r \le 80^{\circ}$	60° < 70	$\theta_r \leq 0$	45° < 60	$\theta_r \le 0$	$\theta_r \le 45^{\circ}$		
<i>H</i> ≥ 20 m	8		7	6	j.	5		4		
$15 \text{ m} \le H < 20 \text{ m}$	7		6	5	i	4		3		
$10 \text{ m} \le H < 15 \text{ m}$	6		5	4		3		2		
$5 \text{ m} \le H < 10 \text{ m}$	5		4	3		2		2		
<i>H</i> < 5 m	4		3	2	2	2		1	A2	
(A3) Instability Classifi $A3_a$ – Mode and scale of Mode of	failure									
failure Scale of failure (volume)	Ravel	ling	Торр	oling	We	edge	P	lanar		
Large $(> 50 \text{ m}^3)$	6		1	0	1	.0		10		
Medium $(5 - 50 \text{ m}^3)$	3		6	,	-	6		6		
Small ( $< 5 \text{ m}^3$ )	2		3	1		3		3		
None	1		1			1		1		
$A3_b$ – Potential for failur	re to occi	ır							A3 = A3	$_a \times A3_b$
Low potential for failure 0.5							12			
High potential for fail	•		1.0			A3				

# (A4) Seepage and Drainage Conditions

Seepage Drainage Provision	Heavy	Moderate	Slight or none
Potential for convergence of runoff at crest area and/or potential for water ingress into open discontinuities	8	6	4
Insufficient or no drainage measures in place to direct water away from the crest area and face of the slope	6	4	2
Orainage measures dequately direct water way from the crest area and face of the slope	4	2	1

<b>(B)</b>	ACTUAL PERFORMANCE (AP)		
(B1)	Signs of Distress		
	(i) Severe	<u>B1</u> 10	
	(ii) Moderate	4	
	(iii) Minor/None	1	B1
(B2)	Instability after Slope Treatment/Formation		
	(i) Documented evidence of past instability (failure volume $\geq 50 \text{ m}^3$ )	<u>B2</u> 10	
	(ii) Documented evidence of past instability (failure volume $< 50 \text{ m}^3$ )	5	
	(iii) Observed evidence of past instability	2	
	(iv) No recorded or observed evidence of past instability	1	B2

( <b>C</b> )	FAC	CILITIES ABOVE CREST OF FEATURE			
	(i)	Type of crest facility (for roads and footpaths, give also the name)		Facility <u>Group</u>	C1
		(refer to Table 2.1 of the main text)		1 (a)	9
				1 (b)	3
	(ii)	Facility Group		2 (a)	2
				2 (b)	1
				3	0.25
	(iii)	Distance (D) from crest of feature to crest facility (refer to Figure 2.1 of the main text)		4	0.002
		,	m	5	0.0002
				'	
				C1	
	(iv)	Vulnerability Factor, C2 (refer to Table 3.1 of		C2	
		the main text)		C2	
<b>(D)</b>	FAC	CILITY AT TOE OF FEATURE			
	(i)	Type of toe facility (for roads and footpaths, give also the name)		Facility Group	D1
		(refer to Table 2.1 of the main text)		1 (a)	9
				1 (b)	2
	(ii)	Espilita Carra		- (-)	3
		Facility Group		2 (a)	2
		racinty Group			
				2 (a)	2
	(iii)	Distance $(L)$ from toe of feature to toe facility		2 (a) 2 (b)	2
	(iii)		m	2 (a) 2 (b) 3	2 1 0.25
	(iii)	Distance $(L)$ from toe of feature to toe facility	m	2 (a) 2 (b) 3 4	2 1 0.25 0.002
	(iii)	Distance $(L)$ from toe of feature to toe facility	m	2 (a) 2 (b) 3 4 5	2 1 0.25 0.002
		Distance (L) from toe of feature to toe facility (refer to Figure 2.1 of the main text)  Shadow angle ( $\omega$ ) from crest of feature to toe	m	2 (a) 2 (b) 3 4	2 1 0.25 0.002
		Distance ( <i>L</i> ) from toe of feature to toe facility (refer to Figure 2.1 of the main text)		2 (a) 2 (b) 3 4 5	2 1 0.25 0.002
	(iv)	Distance ( $L$ ) from toe of feature to toe facility (refer to Figure 2.1 of the main text)  Shadow angle ( $\omega$ ) from crest of feature to toe facility (refer to Figure 2.1 of the main text)		2 (a) 2 (b) 3 4 5	2 1 0.25 0.002
	(iv)	Distance (L) from toe of feature to toe facility (refer to Figure 2.1 of the main text)  Shadow angle ( $\omega$ ) from crest of feature to toe		2 (a) 2 (b) 3 4 5	2 1 0.25 0.002

CALCU	ULATED SCORES			
INSTAE	BILITY SCORE (IS)			
IS = A1	$\times A2 \times A3 \times A4 \times B1 \times B2$		IS	
CONSE	QUENCE SCORE (CS)			
CS = [C]	$1 \times C2 + D1 \times D2] \times K$			
	Probable Scale of Failure Volume	K		
	< 5 m <sup>3</sup>	1		
	5 to 50 m <sup>3</sup>	3		
	$> 50 \text{ m}^3$	5		
			CS	
TOTAL	SCORE (TS)			
TS = IS	$\times$ CS			
			TS	

#### **B.2** Guidelines on Data Collection and Score Computation for Rock Cut Slopes

#### General

- (1) For composite features, i.e. with more than one type of slope feature, the criteria for computation of the Total Score (*TS*) are presented in Figure 2.3 of the main text.
- (2) Geometric parameters of the feature (e.g.  $H_s$ ,  $H_r$ ,  $H_{cw}$ ,  $H_{tw}$ , and  $\theta_r$ ) (see Figure B1) may be obtained from survey plans and site measurements.
- (3) Detailed physical inspection of the features should be carried out using all available access/route.
- (4) Unless stated otherwise, "distance" refers to horizontal distance and "height" refers to vertical height.
- (5) Compute *TS* for each section where there is a potential for a particular mode of failure. If more than one mode of failure is kinematically possible, compute *TS* for each section, and adopt the highest one as the score for the entire feature.
- (6) Details of field mapping and site observation should be recorded using data collection sheets. Sample data collection sheets for rock cut slopes are appended for reference. Inspecting engineers may modify the sheets to suit their specific use. Provide photographic records at each cross-section identified as having potential for a particular mode of failure. The photographs should show the discontinuities characteristics which render the failure mode possible. Provide sketches or overlays to highlight the relevant discontinuity set(s).

#### Factor A1

- (7) Rock slopes that were processed and accepted by GEO (e.g. slopes checked by GEO without outstanding comments and slopes designed by GEO) will not be ranked. Denote these features with AI = 0. Data on these slopes should still be collected.
- (8) The level of geotechnical engineering input should be inferred from databases, files and documentary records kept by GEO and other relevant government departments and organizations, or aerial photographs if necessary.
- (9) Rock slopes with none or little geotechnical engineering input, e.g.
  - pre-1978 slopes
  - post-1978 slopes formed by unauthorized works
  - post-1978 slopes falling outside any engineering project boundary
- (10) Rock slopes with indication of some geotechnical engineering input, e.g.
  - post-1978 slopes without GEO checking records but falling within the boundary of engineering projects
  - slopes assessed as being upto the required safety standard without detailed discontinuity mapping and assessment

- (11) Rock slopes with indication of substantial geotechnical engineering input, e.g.
  - slopes checked by GEO but with outstanding comments

#### Factor A2

(12) Feature height (H) and rock slope angle ( $\theta_r$ ) of the section at which a potential mode of instability exists.

#### Factor A3

- (13) A detailed field inspection is required to identify the probable mode and scale of failure, e.g. ravelling, toppling, planar and wedge failures. In determining the probable mode and scale of failure, due consideration should be given to the characteristics of the discontinuities, i.e. orientation, spacing, roughness and persistence, which render a particular mode of failure kinematically possible.
- (14) Choose "Scale of failure" = "None" if there is no adversely oriented discontinuity set that may lead to instability; or the existing engineering measures in place can effectively mitigate a particular mode of failure, e.g. installation of wire mesh to prevent ravelling failure, or installation of patterned rock bolts to prevent toppling/planar/wedge failure.
- (15) If the slope is concealed by shotcrete/chunam, or some part of the slope is inaccessible for detailed inspection, the characteristics of the discontinuities may be inferred from inspection of adjoining or nearby man-made features and rock exposures. If none of the discontinuity is accessible for inspection, relate the slope performance to the instability classification where appropriate, e.g. if the slope has records of severe signs of distress (BI = 10) or a large scale failure (B2 = 10), adopt a high score in the instability classification.
- (16) Judgment on the potential for failure to occur should be based on an overall assessment of the rock mass and the related environmental factors:
  - high potential for failure to occur, e.g. with steeply dipping and daylighted discontinuities, evidence of progressive deterioration of the slope or the joint conditions, potential build-up of cleft water pressure, or growth of undesirable vegetation, etc.
  - low potential for failure to occur, e.g. with shallow dipping discontinuities, or release surface not present

#### Factor A4

(17) Crest area refers to the area within a horizontal distance of H/2 beyond the crest of the slope.

- (18) In assessing the adequacy of drainage provisions, the overall setting including the site topography, catchment area and environmental factors that are liable to give rise to convergent flow of surface water should be considered.
- (19) The potential for convergent flow of surface water above crest should be determined from topographic plan and/or aerial photographs.
- (20) Staining on or below joints often indicates seepage. When seepage or staining is noted from joints on the slope, its location should be marked on the feature plan.
- (21) If the inspection is being done in the dry season, seepage conditions could be assessed based on water staining on the slope surface.

#### Factors *B1* and *B2*

- (22) Signs of distress are based on site observations, and relevant inspection and maintenance records kept by the maintenance departments.
- (23) Severe signs of distress refer to surficial loosening and small overhanging blocks in several areas of slope, or tension cracks exist along crest of slope, or large overhanging blocks with potential release surfaces visible.
- (24) Moderate signs of distress refer to localised surficial loosening, or small overhanging blocks.
- (25) Minor signs of distress refer to no evidence of surficial loosening.
- (26) Judgment should be made in assessing whether cracked slope cover, damaged channels, etc. are due to inadequate maintenance. If these are due to inadequate maintenance, they should not be regarded as signs of distress. In case of doubt, a conservative assessment should be made.
- (27) Instability after treatment accounts for landslide incidents occurred after the slope was formed or substantially modified to its present configuration and upgrading works have not been carried out on the slope subsequent to the incidents.

#### Factors *C* and *D*

(28) Shadow angle ( $\omega$ ) as shown in Figure 2.1 of the main text should be determined by site measurements and/or from survey plans and sections.

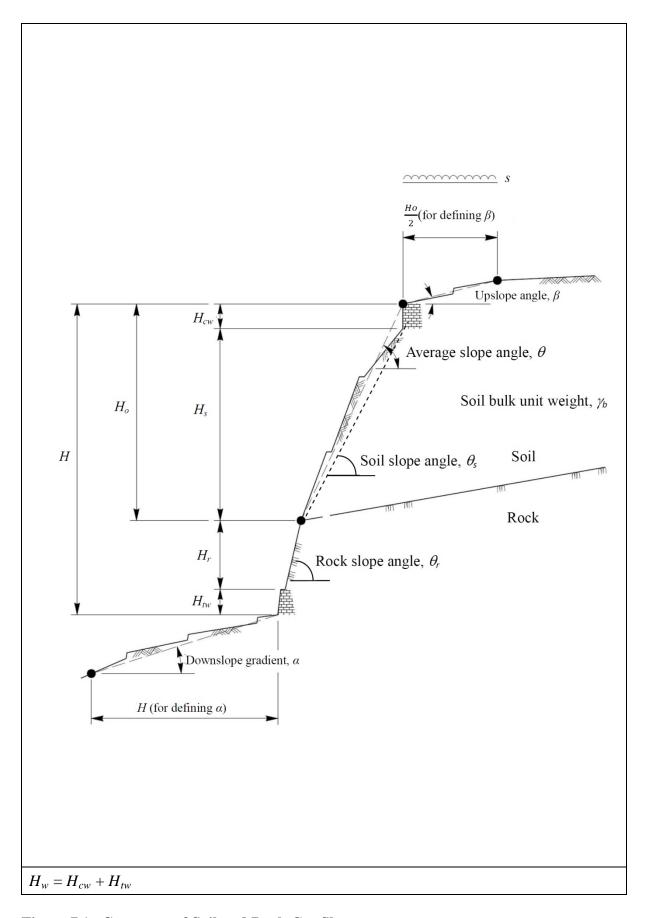


Figure B1 Geometry of Soil and Rock Cut Slopes

# **B.3** Sample Data Collection Sheets for Rock Cut Slopes

FEATURE NO.			(F	Page 1 of )
SECTION:				
Note: Total Score should be computed for ea wedge and planar, and adopt the highe	ch section where there is a potentia est one as the score for the entire fea	l for a particular mode of fa uture	ilure, i.e. ravelling, to	ppling,
Geometry (Figure B1)			$\frac{Ho}{2}(\text{for defining }\beta)$	
Feature Height, H (m)		H <sub>cv</sub> ↓	Upslop	e angle, β
Rock Slope Height, $H_r$ (m)			$\theta$	
Soil Slope Height, $H_s$ (m)	$H_o$	$H_{5}$		
Crest Wall Height, $H_{cw}$ (m)	Н		$ heta_{\scriptscriptstyle S}$	Soil
Toe Wall Height, $H_{tw}$ (m)	<u> </u>		THE THE	Rock
Rock Slope Angle, $\theta_r$ (°)		$H_r$ $\theta_r$		
Soil Slope Angle, $\theta_s$ (°)	<u> </u>	H <sub>rw</sub>		
Average Slope Angle, θ(°)	***************************************	Downslope gradient, α		
Do the dimensions of individual featurin Figure 2.3 of the main text?  • Yes  • N  If yes, number of data collection shee	No	y the requirement of se	eparate Total Scor	e as shown
Affected Facilities (Figure 2.1 and 7	Table 2.1 of the main text)			
Section 1-1	Facility Type	Facility Group	Proximi	ty
Toe			L = ω =	m o
Crest			D =	m
Section 2-2	Facility Type	Facility Group	Proximi	ty
Toe			<i>L</i> = ω =	m o
Crest			D =	m

FEA	TEATURE NO. (Page 2 of )						
PLA	AN AND CRO	SS-SEC	ΓΙΟΝ				
SEC	CTION:	0	1-1 (Most Severe Consequence	<del>?</del> )	0	2-2 (Maximum Feature Height)	
1. I 2. S 3. I	N (1:1000) Feature boundary (SI Section Mark Photo Location and I	Direction	sed Feature Boundary (if applicable)	CROSS-SECTIONS 1. Fully dimensioned 2. Individual sections and 3. Engineering measure	shall be pres. (e.g. r	rovided for each probable mode of failure ock bolts/dowels, shotcrete, buttress & wire mesh)	
5. 5	Signs of distress, if a Signs of seepage, if a Engineering measure	any	bolts/dowels, shotcrete, buttress & wire mesh)				

(Page 3 of )	SITE OBSERVATIONS/FINDINGS						
FEATURE NO.	RAVELLING	TOPPLING	WEDGE	PLANAR			
Rock lithology and nature of discontinuity (see Remark A)							
Dips of discontinuities/line of intersection of discontinuities (°)							
Persistence of discontinuity (m) (i.e. max. dimension of trace length exposed)							
Discontinuity spacing (m)							
Discontinuity roughness and infilling (see Remarks B and C)							
Width of discontinuity aperture (see Remark D)							
Probable scale of failure volume (m <sup>3</sup> )							

# Remarks

_				
	A. Nature of Discontinuity	B. Roughness of Discontinuities	C. Infilling Materials	D. Aperture
	1. Joint	1. Rough	Clean/staining	1. Wide (> 200 mm)
	2. Fault	2. Smooth	2. Strong/Firm materials	2. Moderate (20 – 200 mm)
	3. Tension crack	<ol><li>Slickensided</li></ol>	e.g. decomposed/disintegrated rock	3. Narrow (0 – 20 mm)
	4. Shear Plane		3. Weak/Soft materials	4. Tight (zero)
	5. Foliation		e.g. soil/koalin	
	6. Bedding		4. Others	

Note: If slope face is concealed or part of the slope inaccessible, the characteristics or discontinuities should be inferred from inspection of adjoining/nearby exposed slope areas.

FEATURE NO.							(Page 4 of )	
SLOPE CHARACTERISTICS			SITE O	BSERVATIONS/	FINDIN	GS		
	Signs of Seepage? • Yes • No  If Yes, provide following details							
Seepage Condition (Provide photographic records of signs of seepage and indicate location & extent on plan &	Seepage Location			Copious	1	n of seepage	Stain	
	At or above	e mid-hei	ight					
cross-sections)	Below mid	-height						
	o Other	observat	ions/records	:				
	Location  Crest	Size (mm)	Spacing (m)	Type (e.g. U-cl step chann downpipes or	el,	Adequate Capacity (Y/N)	Remarks	
	Berm							
Drainage Provision	On Slope							
Dramage 1 Tovision	Toe							
	<ul> <li>Potential surface runoff or flow converge onto the crest area due to topography (observed or inferred from topographic plan or aerial photos)</li> <li>Slope located on a drainage line/zone of depression</li> <li>Inadequate surface drainage provision</li> <li>Other observations/records</li> </ul>							
Instability after Slope Formation/Treatment (Provide photographic records of the inferred failure scar and indicate location on plan & cross-sections)	<ul><li>Reported</li><li>Possible</li><li>Estimate</li></ul>	l failure _ failure so d failure	car observed	atobservations:	_ of the s			

FEATURE NO.	(Page 5 of )
SLOPE CHARACTERISTICS	SITE OBSERVATIONS/FINDINGS
	<ul> <li>No indication of any signs of distress</li> <li>Reported signs of distress in inspection or maintenance records</li> </ul>
Signs of Distress  (Provide photographic records of signs of distress and indicate location & extent on plan & cross-section)	<ul> <li>Observed signs of distress (please tick)</li> <li>Tension crack(s) along crest of slope (approx mm wide max)</li> <li>Surficial loosening and small overhanging blocks in several areas</li> <li>Large overhanging block with visible release surface</li> <li>Localised surficial loosening of blocks or small overhanging blocks</li> <li>No noticeable surficial loosening blocks</li> <li>Others:</li> <li>Where severe signs of distress or hazardous movement is noted, appropriate follow-up action should be taken immediately.</li> <li>Judgment should be made in assessing whether cracked slope cover, damaged channels etc. are due to inadequate maintenance, if so, they should not be regarded as signs of distress.</li> </ul>
OTHER OBSERVATIONS/I	REMARKS
INSPECTION DATE:	/ / (dd/mm/yyyy) BY:

FEATURE NO.	(Page 6 of	)
PHOTOGRAPHIC RECORDS		
[Caption]		
PHOTOGRAPHIC RECORDS		
[Caption]		
Notes:		
<ul> <li>(1) Indicate photograph vantage points on plan</li> <li>(2) Add more pages for additional photographic records/sketches</li> </ul>		

# **B.4** Worked Example (Data Collection Sheets)

# FEATURE NO. "Worked Example 2"

(Page 1 of 7)

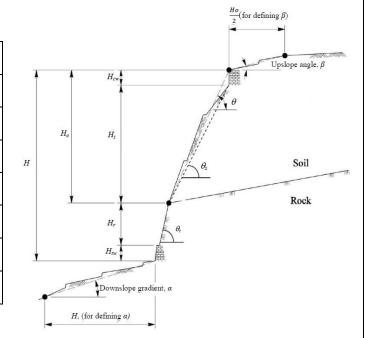
**SECTION:** 

1-1 (Most Severe Consequence)

Note: Total Score should be computed for each section where there is a potential for a particular mode of failure, i.e. ravelling, toppling, wedge and planar, and adopt the highest one as the score for the entire feature

Geometry (Figure B1)

Feature Height, H (m)	10 m
Rock Slope Height, $H_r(m)$	10 m
Soil Slope Height, $H_s$ (m)	_
Crest Wall Height, $H_{cw}$ (m)	_
Toe Wall Height, $H_{tw}$ (m)	_
Rock Slope Angle, $\theta_r$ (°)	75 °
Soil Slope Angle, $\theta_s$ ( $^{\circ}$ )	_
Average Slope Angle, θ(°)	75 °



Do the dimensions of individual feature types at this section satisfy the requirement of separate Total Score as shown in Figure 2.3 of the main text?

o Yes



If yes, number of data collection sheets required for this section:

Affected Facilities (Figure 2.1 and Table 2.1 of the main text)

Section 1 - 1	Facility Type	Facility Group	Proximity
Toe	Residential	1(a)	$L = 2 m$ $\omega = 70^{\circ}$
Crest	Undeveloped Green Belt	5	$D = 0 \mathbf{m}$

Section 2 - 2	Facility Type	Facility Group	Proximity
Toe	_	_	$L = - m$ $\omega = - o$
Crest	_	_	<i>D</i> = — m

# "Worked Example 2" FEATURE NO. (Page 2 of 7) PLAN AND CROSS-SECTION **SECTION:** 1-1 (Most Severe Consequence) 0 2-2 (Maximum Feature Height) 225 UC Moderate seepage 80%287 Potential failure $\sqrt{1}$ wedge 7/x 4 x 1 225 UC 225 UC. Zone of potential ravelling 6 x 4 x 0.4 Unstable block $2 \times 1.5 \times 0.5$ 225 UC <u>Plan</u> (Not to scale)

## PLAN (1:1000)

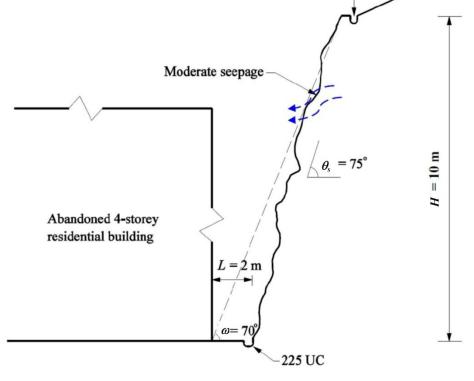
- 1. Feature boundary (SIS) and Revised Feature Boundary (if applicable)
- 2. Section Mark
  3. Photo Location and Direction
  4. Signs of distress, if any
  5. Signs of seepage, if any

- Engineering measures (e.g. rock bolts/dowels, shotcrete, buttress & wire mesh)

## CROSS-SECTIONS

- 1. Fully dimensioned
- 2. Individual sections shall be provided for each probable mode of failure
- 3. Engineering measures. (e.g. rock bolts/dowels, shotcrete, buttress & wire mesh)

# "Worked Example 2" FEATURE NO. (Page 3 of 7) PLAN AND CROSS-SECTION **SECTION:** 1-1 (Most Severe Consequence) 0 2-2 (Maximum Feature Height) Worked example 2 Undeveloped greenbelt 225 UC



Note: No reinforcement or structural support observed on site

# Section 1-1 (Not to scale)

- 1. Feature boundary (SIS) and Revised Feature Boundary (if applicable)
- Section Mark
   Photo Location and Direction
   Signs of distress, if any
   Signs of seepage, if any

- 6. Engineering measures (e.g. rock bolts/dowels, shotcrete, buttress & wire mesh)

# CROSS-SECTIONS

- 1. Fully dimensioned
- 2. Individual sections shall be provided for each probable mode of failure
- 3. Engineering measures. (e.g. rock bolts/dowels, shotcrete,, buttress & wire mesh)

(Page 4 of 7 )	SITE OBSERVATIONS/FINDINGS							
FEATURE NO. "Worked Example 2"	RAVELLING	TOPPLING	WEDGE	PLANAR				
Rock lithology and nature of discontinuity (see Remark A)	Volcanic Rock with Joints	_	Volcanic Rock with Joints	_				
Dips of discontinuities/line of intersection of discontinuities (°)	Multiple sets of sub-vertical joints		45° / 350°, 50° / 340° 90° / 220°, 80° / 287°	_				
Persistence of discontinuity (m) (i.e. max. dimension of trace length exposed)	0.1 - 0.4  m	_	1 – 7 m	_				
Discontinuity spacing (m)	0.1 – 0.4 m	_	1 – 5 m	_				
Discontinuity roughness and infilling (see Remarks B and C)	Rough and staining		Rough and staining	_				
Width of discontinuity aperture (see Remark D)	0 – 20 mm		Narrow to tight					
Probable scale of failure volume (m <sup>3</sup> )	$6 \times 4 \times 0.4 = 9.6 \text{ m}^3$ (H) (W) (D)	_	$7 \times 4 \times 1 = 28 \text{ m}^3$ (H) (W) (D)	_				

# Remarks

A. Nature of Discontinuity B. Roughness of Discontinuities		C. Infilling Materials	D. Aperture	
1. Joint	1. Rough	1. Clean/staining	1. Wide (> 200 mm)	
2. Fault	2. Smooth	2. Strong/Firm materials	2. Moderate (20 – 200 mm)	
3. Tension crack	3. Slickensided	e.g. decomposed/disintegrated rock	3. Narrow (0-20 mm)	
4. Shear Plane		3. Weak/Soft materials	4. Tight (zero)	
5. Foliation		e.g. soil/koalin		
6. Bedding		4. Others		

Note: If slope face is concealed or part of the slope inaccessible, the characteristics or discontinuities should be inferred from inspection of adjoining/nearby exposed slope areas.

FEATURE NO. "Work	ed Exampl	e 2''					(Page 5 of 7)	
SLOPE CHARACTERISTICS	SITE OBSERVATIONS/FINDINGS							
	Signs of See		wing details	<b>√</b> Yes	o No	)		
Seepage Condition  (Provide photographic records of signs of seepage and indicate location & extent on plan & cross-sections)	At or above	-height		Copious  — —	ı	n of seepage ing/damp	Stain  — —	
Drainage Provision	o Slope I  ✓ Inadeq  ✓ Others	ved or info located o uate surf observat : Due 1	ferred from  n a drainage  ace drainage  tions/record  to a large	s catchment exi	el  nto the cor aerial pression	ohotos) v <b>e the roc</b> l	k slope, the	
Instability after Slope Formation/Treatment  (Provide photographic records of the inferred failure scar and indicate location on plan & cross-sections)	<ul> <li>✓ Others observations/records</li> <li>Remarks: Due to a large catchment exist above the rock slope, the 225 UC at crest and toe are considered inadequate</li> <li>○ No indication of any failure occurred after formation or treatment</li> <li>○ Reported failure</li></ul>							

FEATURE NO. "Work	ed Example 2" (Page 6 of 7)
SLOPE CHARACTERISTICS	SITE OBSERVATIONS/FINDINGS
Signs of Distress  (Provide photographic records of signs of distress and indicate location & extent on plan & cross-section)	<ul> <li>No indication of any signs of distress</li> <li>Reported signs of distress in inspection or maintenance records</li> <li>Observed signs of distress (please tick)</li> <li>Tension crack(s) along crest of slope (approx mm wide max)</li> <li>Surficial loosening and small overhanging blocks in several areas</li> <li>Large overhanging block with visible release surface</li> <li>Localised surficial loosening of blocks or small overhanging blocks</li> <li>No noticeable surficial loosening blocks</li> <li>Others: The slope was in poor maintenance conditions, and</li> </ul>
eross section)	potentially unstable blocks and wedges noted in several areas  1. Where severe signs of distress or hazardous movement is noted, appropriate follow-up action should be taken immediately.  2. Judgment should be made in assessing whether cracked slope cover, damaged channels etc. are due to inadequate maintenance, if so, they should not be regarded as signs of distress.

# OTHER OBSERVATIONS/REMARKS

- 1. According to SIFT Report, the slope was formed pre-1978. A GEO Stage 1 study was carried out in 1986.
- 2. The residential building at the toe was abandoned at the time of inspection and the whole site was pending redevelopment.

INSPECTION DATE: 05 / 04 / 2009 (dd/mm/yyyy) BY: PAJ

# FEATURE NO. "Worked Example 2"

(Page 7 of 7)

# PHOTOGRAPHIC RECORDS



V1 General View of the Feature

# PHOTOGRAPHIC RECORDS



**V2** Potential Wedge Failure of the Rock Mass

## Notes:

- (1) Indicate photograph vantage points on plan
- (2) Add more pages for additional photographic records/sketches

# **B.5** Worked Example (*TS* Computation Sheets)

High potential for failure

### FEATURE NO. "Worked Example 2" (refer to Figure B1) (v) Feature Height, $H = H_r + H_s + H_{cw} + H_{tw}$ (i) Rock Slope Height, $H_r = \underline{10}$ m $= \underline{\hspace{1cm} 10 \hspace{1cm}} m$ (vi) Rock Slope Angle, $\theta_r = _{0}$ (ii) Soil Slope Height, $H_s = \underline{\hspace{1cm}} m$ (vii) Soil Slope Angle, $\theta_s =$ (iii) Crest Wall Height, $H_{cw} = \underline{\hspace{1cm}}$ m (iv) Toe Wall Height, $H_{tw} =$ \_\_\_\_m INSTABILITY POTENTIAL (IP) (A1) Level of Geotechnical Engineering Input A1(i) Slopes with none or little geotechnical engineering input 10 3 (ii) Slopes with indication of some geotechnical engineering input 10 A1(iii) Slopes with indication of substantial geotechnical engineering input 1 For rock cut slopes excluded from ranking (see Note 7), denote A1 = 0(A2) Geometry Rock Slope Angle $(\theta_r)$ $\theta_r > 80^{\circ}$ $70^{\circ} < \theta_r \le 80^{\circ} \mid 60^{\circ} < \theta_r \le 70^{\circ} \mid 45^{\circ} < \theta_r \le 60^{\circ}$ $\theta_r \leq 45^{\circ}$ Feature Height (H)8 5 4 $H \ge 20 \text{ m}$ 6 7 6 5 4 3 $15 \text{ m} \le H < 20 \text{ m}$ 5) $10 \text{ m} \le H < 15 \text{ m}$ 6 4 3 2 2 $5 \text{ m} \le H < 10 \text{ m}$ 5 4 3 2 *A2* 5 H < 5 m4 3 2 2 1 (A3) Instability Classification $A3_a$ – Mode and scale of failure Mode of failure Ravelling Planar **Toppling** Wedge Scale of failure (volume) Large ( $> 50 \text{ m}^3$ ) 6 10 10 10 (6)Medium $(5-50 \text{ m}^3)$ 3 6 6 Small ( $< 5 \text{ m}^3$ ) 2 3 3 3 1 1 1 1 None $A3 = A3_a \times A3_b$ $A3_b$ – Potential for failure to occur Low potential for failure 0.5 *A3* 6

(1.0)

# (A4) Seepage and Drainage Conditions

Seepage Drainage Provision	Heavy	Moderate	Slight or none
Potential for convergence of runoff at crest area and/or potential for water ingress into open discontinuities	8	6	4
Insufficient or no drainage measures in place to direct water away from the crest area and face of the slope	6	4	2
Drainage measures adequately direct water away from the crest area and face of the slope	4	2	1

A4 **4** 

# **(B)** ACTUAL PERFORMANCE (AP) (B1) Signs of Distress <u>B1</u> (i) Severe (ii) Moderate 4 (iii) Minor/None **10** B1(B2) <u>Instability after Slope Treatment/Formation</u> <u>B2</u> (i) Documented evidence of past instability (failure volume $\geq 50 \text{ m}^3$ ) 10 (ii) Documented evidence of past instability (failure volume < 50 m<sup>3</sup>) 5 (iii) Observed evidence of past instability 2 (iv) No recorded or observed evidence of past instability 1 *B*2 2

(C)	FA(	CILITIES ABOVE CREST OF FEATURE			
	(i)	Type of crest facility (for roads and footpaths, give also the name)	Undeveloped	Facility Group	C1
		(refer to Table 2.1 of the main text)	green belt	1 (a)	9
				1 (b)	3
	(ii)	Facility Group	5	2 (a)	2
				2 (b)	1
		Di		3	0.25
	(111)	Distance (D) from crest of feature to crest facility (refer to Figure 2.1 of the main text)	0 m	4	0.002
			V III	5	0.0002
				_	
				CI	0.0002
	(iv)	Vulnerability Factor, C2 (refer to Table 3.1 of the main text)		C2 [	0.15
( <b>D</b> )	<b>FA</b> (i)	Type of toe facility (for roads and footpaths, give also the name)	Davidan Cal	Facility Group	DI
		(refer to Table 2.1 of the main text)	Residential	1 (a)	9
	(::\	Facility Crown		1 (b)	3
	(11)	Facility Group	1(a)	2 (a)	2
				2 (b)	1
	(iii)	Shadow angle ( $\omega$ ) from crest of feature to toe		3	0.25
	(111)	facility (refer to Figure 2.1 of the main text)	70 °	4	0.002
				5	0.0002
	(iv)	Distance $(L)$ from toe of feature to toe facility (refer to Figure 2.1 of the main text)	2 m		9
	(v)	Vulnerability Factor, D2 (refer to Table 3.2 of the main text)		D2	0.45

CALCU	LATED SCORES				
INSTAB	ILITY SCORE (IS)				
IS = A1	$\times A2 \times A3 \times A4 \times B1 \times B2$			IS	24000
CONSE	QUENCE SCORE (CS)				
CS = [C.	$1 \times C2 + D1 \times D2] \times K$				
	Probable Scale of Failure Volume	K			
	< 5 m <sup>3</sup>	1			
	5 to 50 m <sup>3</sup>	3			
	$> 50 \text{ m}^3$	5			
			K = 3	CS	12.15
				L	
TOTAL	SCORE (TS)				
TS = IS	× CS			TS	291600

# Appendix C

Details of NPRS for Fill Slopes

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# **List of Figure**

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# **C.1** Total Score (TS) Computation Sheets for Fill Slopes

FEATURE NO.	SECTION:  o 1-1 (Most Severe Consequence)  o 2-2 (Maximum Feature Height)
(refer to Figure C1)	
(i) Fill Slope Height, $H_f = $ m	(iv) Feature Height, $H = \underline{\hspace{1cm}} m$
(ii) Crest Wall Height, $H_{cw} = $ m	(v) Fill Slope Angle, $\theta_f$ = °
(iii) Toe Wall Height, $H_{tw} = $ m	(vi) Average Slope Angle, $\theta = $ $^{\circ}$
INSTABILITY SCORE (IS)	
(A) INSTABILITY POTENTIAL (IP)	
(A1) Level of Geotechnical Engineering Input	A.1
(i) Slopes with none or little geotechnical engine	eering input $\frac{AI}{10}$
(ii) Slopes with indication of some geotechnical of	engineering input 3
(iii) Slopes with indication of substantial geotechi	nical engineering input 1
For fill slopes excluded from ranking (see Note 7)	, denote $AI = 0$
(A2) Sliding and Minor Washout Failure	$A2 = A2_a \times A2_b \times A2_c \times A2_d \times A2_e =$
(A2 <sub>a</sub> ) Geometry (From Figure C1) SI = 32 S2 = 16	$(A2_c)$ Surface Drainage Provision No = 2 Yes = 1
S3 = 8 $S4 = 4$	(A2 <sub>d</sub> ) Signs of Seepage
S5 = 2 $S6 = 1$	Yes = 2 $No = 1$
(A2 <sub>b</sub> ) Type of Surface Cover Bare = 4 Vegetated = 3 Chunam = 1.5 Shotcrete = 1	(A2 <sub>e</sub> ) Potential Leaking Water-carrying Services Leaking = 2 Presence = 1.5 None = 1
(A3) <u>Liquefaction Failure</u>	$A3 = \frac{1}{4} \times A2 \times A3_a \times A3_b =$
(A3 <sub>a</sub> ) Feature Height, $H$ (m) $H \ge 30 = 4$ $20 \ge H < 30 = 3$ $10 \ge H < 20 = 1$ H < 10 = 0.5	$(A3_b)$ Type of Surface Cover Bare = 1.3 Vegetated = 1.1 Chunam = 0.5 Shotcrete = 0.25

(A4) Major Was	shout Fa	<u>iilure</u>		A	$A4 = (A2)^{1}$	(A4) <u>Major Washout Failure</u> $A4 = (A2)^{1/3} \times A4_a \times A4_b \times A4_c \times A4_d \times A4_e \times A4_f \times A4_g \times A4_h =$						
$(A4_a)$ Catchment Characteristics: Topographic $(A4_b)$ Type of Crest Facility												
Setting and Size of Catchment							<b>.</b>	Platform &	Catch-	Minor Developmen	t Natural	
Topographic				ment (m	n <sup>2</sup> )		Road	Urban Development	Water	e.g. Rural Footpath	Hillside	
Setting	≤ 100	100 - 500	500 - 1000	1000- 10000	>10000		1.0	0.5	0.25	0.10	0.05	
Traverse Drainage	2	4	8	16	32	(11	) Valu	me of Fill Boo	1. (m <sup>3</sup> )			
Line	2	4	0	10	32	(A4	<ul> <li>voiu</li> <li>≤ 100</li> </ul>		500	1000 -	>10000	
Adjacent to Drainage Line	2	3	6	12	24		0.10		-1000 0.5	10000	2	
Traverse Topographic Depression	1	2	4	8	16	(A4	d) <u>Chai</u>	nnelisation of	<u>Debris</u>	Yes = No =		
Adjacent to Topographic Depression	1	2	3	6	12	(A4		ion and Entrai g Debris Trail	<u>nment</u>	Yes = No =		
Planar Slope	0.5	1	3	5	10	(A4)	) Spre	ad of Debris		Yes = No =		
Spur	0.5	1	2	4	8	(A4 <sub>1</sub>	g) <u>Unst</u>	able Terrain		Yes = No =		
$(A4_h)$ Mas							onry Wall at C	<u>rest</u>				
	Wall Height ≥ 3 m 2.0											
	Wall Height < 3 m 1.5											
						_ 1	No Mas	onry Wall		1.0		
(B) ACTUAL	PERFO	)RMA	NCE (	<b>AP</b> )								
(B1) Signs of Di	istress								D 1			
(i) Severe	e								<u>B1</u> 10			
(ii) Moder	rate								4	B1		
(iii) Minor	/None								1			
(B2) Instability	after Slo	pe For	mation	/Treatn	nent				<u>B2</u>			
(i) Massi	ve failu	res ( > :	500 m <sup>3</sup>	)					10			
	or repe ords of				of distres	SS			5	na		
(iii) Minor	failure	or reco	ords of	previou	s modera	te sign	s of dis	tress	2	B2		
(iv) No failure or records of previous minor signs of distress 1												

INSTABILITY SCORE (IS)		
$IS_1$ = Instability Score for Sliding and Minor Washout = $A1 \times A2 \times B1 \times B2$	$IS_I$	
$IS_2$ = Instability Score for Liquefaction = $A1 \times A3 \times B1 \times B2$	$IS_2$	
$IS_3$ = Instability Score for Major Washout = $A1 \times A4 \times B1 \times B2$	$IS_3$	

COI	NSEQUENCE SCORE (CS)		
(C)	FACILITY ABOVE CREST OF FEATURE		
	(i) Type of crest facility (for roads and footpaths, give also the name) (refer to Table 2.1 of the main text)		Facility
	(ii) Facility Group		2 (a) 2 2 (b) 1 3 0.25
	(iii) Distance (D) from crest of feature to crest facility (refer to Figure 2.1 of the main text)	m	4 0.002 5 0.0002
	(iv) Vulnerability Factor, C2 (refer to Table 5.1		CI
	of the main text)		C2 <sub>1</sub> C2 <sub>2</sub> C2 <sub>3</sub>
(D)	FACILITY AT TOE OF FEATURE		
	(i) Type of toe facility (for roads and footpaths, give also the name) (refer to Table 2.1 of the main text)		Facility
	(ii) Facility Group		2 (a) 2 2 (b) 1
	(iii) Distance ( <i>L</i> ) from toe of feature to toe facility (refer to Figure 2.1 of the main text)	m	3 0.25 4 0.002 5 0.0002

<ul> <li>(iv) Shadow angle (ω) from crest of feature to toe facility (refer to Figure 2.1 of the main text)</li> <li>(v) Vulnerability Factor, D2 (refer to Table 5.2 of the main text)</li> </ul>	0	$D1$ $D2_1$ $D2_2$ $D2_3$
CONSEQUENCE SCORE (CS)		
$CS_i = (C1 \times C2_i + D1 \times D2_i) \times H$		
Sliding and minor washout failure, $i = 1$		
Liquefaction failure, $i = 2$		
Major washout failure, $i = 3$		
		$CS_1$
		$CS_2$
		$CS_3$
CALCULATED SCORES		

TS

TOTAL SCORE (TS)

 $TS = \sum_{i=1}^{3} IS_i \times CS_i$ 

# C.2 Guidelines on Data Collection and Score Computation for Fill Slopes

# General

- (1) For composite features, i.e. with more than one type of slope feature, the criteria for computation of the Total Score (*TS*) are presented in Figure 2.4 of the main text.
- (2) If H of Section  $1-1 \ge 75\%$  of H of Section 2-2, consider Section 1-1 (i.e. in terms of most severe consequence) in calculating the scores. Otherwise, both Sections 1-1 and 2-2 (in terms of maximum feature height, H) should be considered.
- (3) Geometric parameters of the feature (e.g.  $H_f$ ,  $H_{cw}$ ,  $H_{tw}$  and  $\theta_f$ ) (see Figure C1) may be obtained from survey plans and site measurements.
- (4) Detailed physical inspection on the features should be carried out using all available access/route.
- (5) Unless stated otherwise, "distance" refers to horizontal distance and "height" refers to vertical height.
- (6) Details of field mapping and site observation should be recorded using data collection sheets. Sample data collection sheets for fill slopes are appended for reference. Inspecting engineers may modify the sheets to suit their specific use. Provide photographic records of the overview of the features and facilities affected. The photographic records should also include details of site observations to substantiate the factors adopted in the calculation.

# Factor A1

- (7) Fill slopes that were processed and accepted by GEO (e.g. slopes checked by GEO without outstanding comments and slopes designed by GEO) will not be ranked. Denote these features with AI = 0. Data on these slopes should still be collected.
- (8) The level of geotechnical engineering input should be inferred from databases, files and documentary records kept by GEO and other relevant government departments and organizations, or aerial photographs if necessary.
- (9) Fill slopes with none or little geotechnical engineering input, e.g.
  - pre-1978 slopes
  - post-1978 slopes formed by unauthorized works
  - post-1978 slopes falling outside any engineering project boundary
- (10) Fill slopes with indication of some geotechnical engineering input, e.g.
  - post-1978 slopes without GEO checking records but falling within the boundary of engineering projects
  - slopes assessed as being upto the required safety standard without site specific ground investigation and laboratory testing

- (11) Fill slopes with indication of substantial geotechnical engineering input, e.g.
  - slopes checked by GEO but with outstanding comments

# Factors A2 to A3

(12) Feature Height (*H*) refers to the height of a fill slope including the height of the crest wall and half of the height of the toe wall (refer to Figure C1).

# Factor A4

- (13) Catchment Characteristics Topographic Setting and Size of Catchment, should be based on SIFT Report. If data are not available, default value 32 for type of crest facility being a road or a catchwater; and 12 for other types of crest facility are suggested.
- (14) Volume of Fill Body should be estimated from survey map, field measurement, or aerial photos. Information from SIFT Report may be used, if available.
- (15) Channelisation of Debris should be based on SIFT Report. If data are not available, default value 0.5 is suggested.
- (16) Erosion and Entrainment along Debris Trail should be based on SIFT Report. If data are not available, default value 1.0 is suggested.
- (17) Spread of Debris should be based on SIFT Report. If data are not available, default value 1.0 is suggested.
- (18) Unstable Terrain should be based on GASP Reports. Unstable terrain refers to the presence of the following between the fill feature and toe facilities: (i) zones of general instability associated with predominantly colluvial terrain or insitu terrain, and (ii) instability on disturbed terrain.

# Factors B1 and B2

- (19) Signs of distress are based on site observations, and relevant inspection and maintenance records.
- (20) Severe signs of distress refer to signs of slope movement, e.g. large tension cracks behind crest, significant distortion of channels and berms, severe cracking and bulging, subsidence of slope crest or slope surface. These tell-tale signs should be examined in a holistic manner to determine if they are indicative of slope movement. Where there are severe signs of distress or documented evidence of continuing hazardous movement, immediate action should be taken. Examples of severe signs of distress are attached in Appendix F of this report.
- (21) Moderate signs of distress refer to signs of extensive minor defects, e.g. cracking of slope cover and damaged channels.

- (22) Judgment should be made in assessing whether cracked slope cover, damaged channels, etc. are due to inadequate maintenance. If these are due to inadequate maintenance, they should not be regarded as signs of distress. In case of doubt, a conservative assessment should be made.
- (23) Instability after treatment accounts for landslide incidents occurred after the slope was formed or substantially modified to its present configuration and upgrading works have not been carried out on the slope subsequent to the incidents.

# Factors *C* and *D*

(24) Shadow angle ( $\omega$ ) as shown in Figure 2.1 of the main text should be determined by site measurements and/or from survey plans and sections.

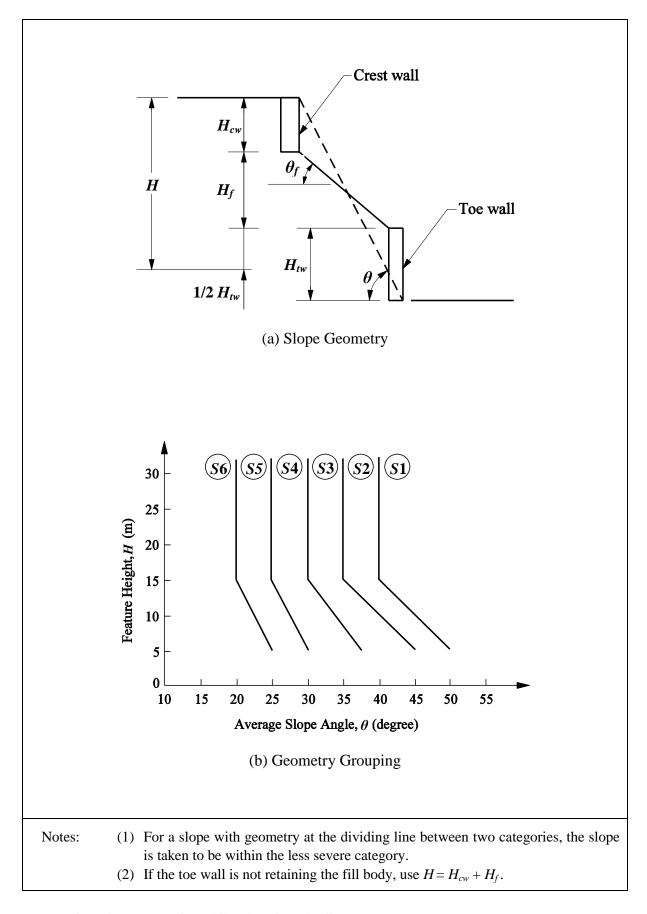


Figure C1 Geometry Classification for Fill Slopes

# **C.3** Sample Data Collection Sheets for Fill Slopes

SECTION: O 1-1 (Most Severe Consequence) O 2-2 (Maximum Feature Heigheigh Check if $H_1 \ge 75\%$ x $H_2$ . If yes, consider Section 1-1 only; If No, consider both Section 1-1 and 2-2  Geometry (Figure C1)  Crest wall $H_{cw}$ $H_{fw}$ Toe wall	nt)
$H_{cw}$ $H_{fw}$ $H_{fw}$ $H_{fw}$ $H_{fw}$ $H_{fw}$ $H_{fw}$ $H_{fw}$ $H_{fw}$	
$lackbr{h}$	
$1/2H_{tw}$ $\downarrow$ $\downarrow$ $\downarrow$ $\downarrow$ $\downarrow$	$\neg$
Geometrical Data Section 1-1 Section 2-2	
Fill Height, $H_f$ (m)	
Crest Wall Height, $H_{cw}$ (m)	
Toe Wall Height, $H_{tw}$ (m)	
Feature Height, H (m)	
Fill Slope Angle, $\theta_f$ (°)	
Average Slope Angle, θ(°)	
Do the dimensions of individual feature types satisfy the requirement of separate Total Score as shown in Figure of the main text?  O Yes O No  If yes, number of data collection sheets required for this section	.4
Affected Facilities (Figure 2.1 and Table 2.1 of the main text)	
Section 1-1 Facility Type Facility Group Proximity	
Toe	
Crest $D = m$	
Section 2-2 Facility Type Facility Group Proximity	
Toe	
Crest $D = m$	

FEATURE NO.					(Page 2 of	)
PLAN AND CR	OSS-SEC	TION				
SECTION:	0	1-1 (Most Severe Consequ	ience)	0	2-2 (Maximum Feature Height)	
Section Mark    Photo Location and    Signs of distress, if	Direction	ed Feature Boundary (if applicable)	CROSS-SECTIONS  1. Fully dimension 2. Existing enginee (e.g. recompaction)	ed ering measi	ures ls, grillage beams & shotcrete)	
<ul><li>5. Signs of seepage, if</li><li>6. Engineering measu</li></ul>	res (e.g. recon	npaction, soil nails, grillage beams & sho	otcrete)			

FEATURE NO.		(Page 3 of )						
SLOPE CHARACTERISTICS	SITE OBSERVATIONS/FINDINGS							
Surface Cover	Surface cover with         % (including grass/shrub           O Chunam         %           O Concrete         % (including shotcrete or           O Bare surface         %           O Others         %							
	I Size I Spacing I	Adequate Capacity (Y/N)						
Surface Drainage Provision	Crest  Berm  On Slope  Toe  O Potential surface runoff converge onto the crest area due or inferred from topographic plan or aerial photos)  Slope located on a drainage line/zone of depression  Inadequate surface drainage evident by surface erosion or							
	<ul> <li>Inadequate surface drainage evident by surface erosion or erosion green on the original of the or</li></ul>							
Signs of Seepage (Provide photographic	If Yes, provide following details  Condition o Seepage Location							
records of signs of seepage and indicate location & extent on plan & cross-sections)	At or above mid-height  Below mid-height  Other observations/records:							
Water-carrying Services	Indication of presence of water-carrying services:  o Exposed water main within crest area/on slope o Valve(s) of water main within crest area/on slope o Manhole cover(s) within crest area/on slope o None of the above							

FEATURE NO. (Page 4 of ) SLOPE SITE OBSERVATIONS/FINDINGS **CHARACTERISTICS** Provide the following data based on SIFT Report on the slope: Size of Catchment: m<sup>2</sup> Topographic Setting: Traverse drainage line Adjacent to drainage line Traverse topographic depression **Catchment Characteristics** o Adjacent to topographic depression Planar slope Spur If the required data are not available in SIFT report, adopt the following default values: 1. A maximum score of 32 should be taken for factor A4a if crest facility is a road or a catchwater. 2. Otherwise, a score of 12 should be adopted. Volume of fill body estimated by: o SIFT Report Volume of Fill Body o Field measurement (if SIFT data are not available) API Estimated volume of fill body: \_\_\_\_\_ m<sup>3</sup> Provide data based on SIFT Report on the slope: In case of failure, channelization of debris flow is possible: Channelisation of Debris o Yes o No If the required data are not available in SIFT report, then No should be assumed. Provide data based on SIFT Report on the slope: In case of failure, erosion and entrainment is possible along the run-out path of the **Erosion and Entrainment** debris flow: along Debris Trail o Yes o No If the required data are not available in SIFT report, then **No** should be assumed. Provide data based on SIFT Report on the slope: In case of failure, spread of debris is possible: Spread of Debris o Yes o No If the required data are not available in SIFT report, then **No** should be assumed. Obtain terrain classification for the area(s) between the slope and toe facilities based on relevant GASP Reports Zones of general instability associated with predominantly colluvial terrain or Unstable Terrain in-situ terrain, and Instability on disturbed terrain

If terrain between the slope and toe facilities meets both of the above criteria, the terrain

should be classified as "Unstable".

FEATURE NO.	(Page 5 of )
SLOPE CHARACTERISTICS	SITE OBSERVATIONS/FINDINGS
	<ul> <li>No indication of any signs of distress</li> <li>Reported signs of distress in inspection or maintenance records</li> </ul>
Signs of Distress  (Provide photographic records of signs of distress and indicate location & extent on plan & cross-sections)	<ul> <li>Observed signs of distress (please tick)</li> <li>Large tension cracks behind crest (approx mm wide)</li> <li>Significant distortion/damage of channels and berms</li> <li>Severe cracking and bulging of hard surfacing</li> <li>Subsidence inside crest area or on slope surface</li> <li>Extensive cracking of slope cover</li> <li>Isolated minor cracking of slope cover/Isolated cracking of channels</li> <li>Others:</li> <li>Where severe signs of distress or hazardous movement is noted, appropriate follow-up action should be taken immediately.</li> <li>Judgment should be made in assessing whether cracked slope cover, damaged channels etc. are due to inadequate maintenance, if so, they should not be</li> </ul>
Instability after Slope Formation/Treatment  (Provide photographic records of the inferred failure scar and indicate location on plan &	regarded as signs of distress.  O No indication of any failure occurred after formation or treatment O Reported failure
cross-sections) OTHER OBSERVATIONS/F	Debris observed on site/Other observations:  REMARKS
INSPECTION DATE:	/ / (dd/mm/yyyy) BY:

FEATURE NO.	(Page 6 of	)
PHOTOGRAPHIC RECORDS		
[Caption]		
PHOTOGRAPHIC RECORDS		
[Caption]		
Notes:		
(1) Indicate photograph vantage points on plan (2) Add more pages for additional photographic records/sketches		

# **C.4** Worked Example (Data Collection Sheets)

# FEATURE NO. "Worked Example 3"

(Page 1 of 7)

**SECTION:** 

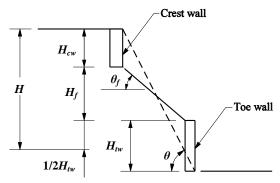
 $\mathbf{N}$ 

1-1 (Most Severe Consequence)

O 2-2 (Maximum Feature Height)

Check if  $H_1 \ge 75\%$  x  $H_2$ . If yes, consider Section 1-1 only; If No, consider both Section 1-1 and 2-2

Geometry (refer to Figure C1)



Geometrical Data	Section 1-1	Section 2-2
Fill Height, $H_f$ (m)	13 m	_
Crest Wall Height, $H_{cw}$ (m)	_	_
Toe Wall Height, $H_{tw}$ (m)	_	_
Feature Height, H (m)	13 m	_
Fill Slope Angle, θ <sub>f</sub> (°)	40 °	_
Average Slope Angle, θ(°)	40 °	_

Do the dimensions of individual feature types satisfy the requirement of separate Total Score as shown in Figure 2.4 of the main text?

o Yes

**√** No

If yes, number of data collection sheets required for this section

\_

Affected Facilities (refer to Figure 2.1 and Table 2.1 of the main text)

Section 1-1	Facility Type	Facility Group	Proximity	
Toe	Densely-used Playground	3	$L = 0 \text{ m}$ $\omega = 40 ^{\circ}$	
Crest	Open Car Park	3	D = 1 m	

Section 2-2	Facility Type	Facility Group	I	Proximity	
Toe		_	<i>L</i> = ω =		m o
Crest		_	D=	_	m

# FEATURE NO. "Worked Example 3" (Page 2 of 7) PLAN AND CROSS-SECTION **SECTION:** 1-1 (Most Severe Consequence) 0 2-2 (Maximum Feature Height) Inferred failure scar estimated volume = $10 \text{ m}^3$ 600 SC 400 SC 150 UC 375 SC Minor erosion <u>Plan</u> (Not to scale)

- PLAN (1:1000)

  1. Feature boundary (SIS) and Revised Feature Boundary (if applicable)
  2. Section Mark
  3. Photo Location and Direction
  4. Signs of distress, if any
  5. Signs of seepage, if any
  6. Engineering measures (e.g. recompaction, soil pails or illustration) Signs of seepage, if any Engineering measures (e.g. recompaction, soil nails, grillage beams & shotcrete)

## CROSS-SECTIONS

- Fully dimensioned
   Existing engineering measures
   (e.g. recompaction, soil nails, grillage beams & shotcrete)

# FEATURE NO. "Worked Example 3"

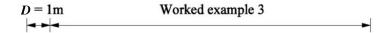
(Page 3 of 7)

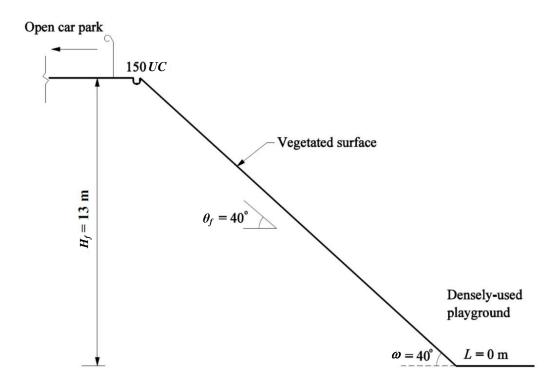
# PLAN AND CROSS-SECTION

**SECTION:** 

1-1 (Most Severe Consequence)

0 2-2 (Maximum Feature Height)





Note: No reinforcement or structural support observed on site

Section 1-1 (Not to scale)

## Notes:

- Engineering measures (e.g. recompaction, soil nails, grillage beams & shotcrete)

# 1. Feature boundary (SIS) and Revised Feature Boundary (if applicable) 2. Section Mark 3. Photo Location and Direction 4. Signs of distress, if any 5. Signs of seepage, if any 6. Engineering measures (e.g. recompaction, soil pails, arithmetically applicable)

- CROSS-SECTIONS
- Fully dimensioned
   Existing engineering measures
   (e.g. recompaction, soil nails, grillage beams & shotcrete)

FEATURE NO. "Worked Example 3"				(Page 4 of 7)			
SLOPE CHARACTERISTICS	SITE OBSERVATIONS/FINDINGS						
Surface Cover	Chu O Cor	getation unam ncrete re surface	10	% (including s			d material)
	Location	Size (mm)	Spacing (m)	Type (e.g. U-char step channel, downpipes or dit		Adequate Capacity (Y/N)	Remarks
	Crest	150	_	U-channel		Y	Lined
	Berm		_	_			_
Surface Drainage Provision	On Slope	600	_	Step-channo	el	Y	Lined
	Toe     350     —     U-channel     Y     Lined       ○ Potential surface runoff converge onto the crest area due to topography (observed or inferred from topographic plan or aerial photos)       ○ Slope located on a drainage line/zone of depression       ○ Inadequate surface drainage evident by surface erosion or erosion gully, etc.       ○ Other observations/records						
Signs of Seepage	Signs of Seepage?  If Yes, provide following details  Seepage Location			Condition of seepage			
(Provide photographic records of signs of seepage			Copious	Trickling/damp Stain		Stain	
and indicate location & extent on plan &	At or above	mid-hei	ght				
cross-sections)	Below mid-height						
	Other observations/records:						
Water-carrying Services	<ul> <li>Expose</li> <li>Valve(</li> <li>Manho</li> <li>None o</li> <li>Others</li> <li>Signs of leak</li> </ul>	ed water s) of wat ole covere of the abo : cage? Yes	main within er main with (s) within crove	arrying services : crest area/on slope nin crest area/on slope est area/on slope  ition of leakage	pe		

FEATURE NO. "Work	ed Example 3" (Page 5 of 7)			
SLOPE CHARACTERISTICS	SITE OBSERVATIONS/FINDINGS			
Catchment Characteristics	Provide the following data based on SIFT Report on the slope:  Size of Catchment:<100m²  Topographic Setting:  Traverse drainage line  Adjacent to drainage line  Traverse topographic depression  Adjacent to topographic depression  Planar slope  Spur  If the required data are not available in SIFT report, adopt the following default values:  A maximum score of 32 should be taken for factor A4a if crest facility is a road or a catchwater.  Cherwise, a score of 12 should be adopted.			
Volume of Fill Body	Volume of fill body estimated by:  SIFT Report  Field measurement (if SIFT data are not available)  API  Estimated volume of fill body:m <sup>3</sup>			
Channelisation of Debris	Provide data based on SIFT Report on the slope: In case of failure, channelization of debris flow is possible:  O Yes  No  If the required data are not available in SIFT report, then No should be assumed.			
Erosion and Entrainment along Debris Trail	Provide data based on SIFT Report on the slope:  In case of failure, erosion and entrainment is possible along the run-out path of the debris flow:  O Yes  No  If the required data are not available in SIFT report, then No should be assumed.			
Spread of Debris	Provide data based on SIFT Report on the slope: In case of failure, spread of debris is possible:  Yes  No If the required data are not available in SIFT report, then No should be assumed.			
Unstable Terrain	Obtain terrain classification for the area(s) between the slope and toe facilities based on relevant GASP Reports  O Zones of general instability associated with predominantly colluvial terrain or in-situ terrain, and  O Instability on disturbed terrain  If terrain between the slope and toe facilities meets both of the above criteria, the terrain should be classified as "Unstable".			

FEATURE NO. "Worke	ed Example 3" (Page 6 of 7)
SLOPE CHARACTERISTICS	SITE OBSERVATIONS/FINDINGS
Signs of Distress  (Provide photographic records of signs of distress and indicate location & extent on plan & cross-sections)	<ul> <li>No indication of any signs of distress</li> <li>Reported signs of distress in inspection or maintenance records</li> <li>Observed signs of distress (please tick)</li> <li>Large tension cracks behind crest (approx mm wide)</li> <li>Significant distortion/damage of channels and berms</li> <li>Severe cracking and bulging of hard surfacing</li> <li>Subsidence inside crest area or on slope surface</li> <li>Extensive cracking of slope cover</li> <li>Isolated minor cracking of slope cover/Isolated cracking of channels</li> <li>Others:</li> <li>Where severe signs of distress or hazardous movement is noted, appropriate follow-up action should be taken immediately.</li> <li>Judgment should be made in assessing whether cracked slope cover, damaged channels etc. are due to inadequate maintenance, if so, they should not be regarded as signs of distress.</li> </ul>
Instability after Slope Formation/Treatment  (Provide photographic records of the inferred failure scar and indicate location on plan & cross-sections)	<ul> <li>No indication of any failure occurred after formation or treatment</li> <li>Reported failure</li></ul>
OTHER OBSERVATIONS/F	REMARKS
According to SIFT Rep 1963 and 1968.	port, the slope was formed before 1949 and was modified between
INSPECTION DATE:	02 / 05 / 2009 (dd/mm/yyyy) BY: <b>PAJ</b>

## FEATURE NO. "Worked Example 3"

(Page 7 of 7)

## PHOTOGRAPHIC RECORDS



V1 Overview of the Slope

## PHOTOGRAPHIC RECORDS



V2 General View of the Crest Area

#### Notes:

- (1) Indicate photograph vantage points on plan
- (2) Add more pages for additional photographic records/sketches

## **C.5** Worked Example (*TS* Computation Sheets)

FEATURE NO. "Worked Example 3"	SECTION: 1-1 (Most Severe Consequence)  O 2-2 (Maximum Feature Height)
(refer to Figure C1)	
(i) Fill Slope Height, $H_f = \underline{13}$ m	(iv) Feature Height, $H = 13$ m
(ii) Crest Wall Height, $H_{cw} = \underline{0}$ m	(v) Fill Slope Angle, $\theta_f = 40^{\circ}$
(iii) Toe Wall Height, $H_{tw} = $ m	(vi) Average Slope Angle, $\theta = $ 40 °
INSTABILITY SCORE (IS)	
(A) INSTABILITY POTENTIAL (IP)	
(A1) <u>Level of Geotechnical Input</u> (i) Slopes with none or little geotechnical engine	ering input $\frac{AI}{10}$
(ii) Slopes with indication of some geotechnical e	engineering input 3
(iii) Slopes with indication of substantial geotechr For fill slopes excluded from ranking (see Note 7),	AI 10
(A2) Sliding and Minor Washout Failure	$A2 = A2_a \times A2_b \times A2_c \times A2_d \times A2_e = $ $48$
(A2 <sub>a</sub> ) Geometry (From Figure C1)	(A2 <sub>c</sub> ) <u>Surface Drainage Provision</u>
S1 = 32 S2 = 16 S3 = 8	$ No = 2  Yes = 1  $ $ A2_c = 1 $
S4 = 4 $S5 = 2$	$(A2_d)$ <u>Signs of Seepage</u> Yes = 2
$S6 = 1   A2_a = 16$	$No = 1   A2_d = 1$
(A2 <sub>b</sub> ) Type of Surface Cover Bare = 4 Vegetated = 3	(A2 <sub>e</sub> ) <u>Potential Leaking Water-carrying Services</u> Leaking = 2 Presence = 1.5
Chunam = 1.5 Shotcrete = 1 $A2_b = 3$	None = 1 $A2_e = 1$
(A3) <u>Liquefaction Failure</u>	$A3 = \frac{1}{4} \times A2 \times A3_a \times A3_b =$ <b>13.2</b>
(A3 <sub>a</sub> ) Feature Height, $H$ (m) $H \ge 30 = 4$ $20 \ge H < 30 = 3$ $10 \ge H < 20 = 1$ $H < 10 = 0.5$ $A3_a = 1$	$(A3_b) \  \  \frac{\text{Type of Surface Cover}}{\text{Bare} = 1.3} \\ \text{Vegetated} = 1.1 \\ \text{Chunam} = 0.5 \\ \text{Shotcrete} = 0.25 \\ A3_b = \textbf{1.1}$

(A4) <u>Major Washout Failure</u> $A4 = (A2)^{1/3} \times A4_a \times A4_b \times A4_c \times A4_d \times A4_e \times A4_f \times A4_g \times A4_h = 0.5$												
(A4 <sub>a</sub> ) <u>Catchment Characteristics : Topographic</u>					(A4	b) Type	e of	Crest Facil	<u>ity</u>			
Setting an	d Size o	of Catel	<u>hment</u>					Pl	atform &	Catch-	Minor Developmen	t Natural
Topographic				ment (m	n <sup>2</sup> )		Road	De	Urban velopment	Water	e.g. Rural Footpath	Hillside
Setting	≤ 100	100 - 500	500 - 1000	1000- 10000	>10000		1.0		0.5	0.25	0.10	0.05
Traverse Drainage	2	4	8	16	32	(A4	c) <u>Volu</u>	ıme	of Fill Bod	y (m <sup>3</sup> )		$A4_b = 0.5$
Line							≤ 100	0	100 –500	500 -1000	1000 - 10000	>10000
Adjacent to Drainage Line	2	3	6	12	24		0.10	)	0.25	0.5	1	2
Traverse Topographic Depression	1	2	4	8	16	(A4	<sub>d</sub> ) <u>Chai</u>	<u>nnel</u>	isation of I	<u>Debris</u>	Yes = No =	
Adjacent to Topographic Depression	1	2	3	6	12	(A4			and Entrainebris Trail	<u>nment</u>	Yes = No =	2.0
Planar Slope	0.5	1	3	5	10	$(A4_{f}) \underline{Spread of Debris} Yes = 0$ $No = 1$			0.5			
Spur	0.5	1	2	4	8	(A4 <sub>g</sub> ) <u>Unstable Terrain</u>			Yes = No =	2.0		
					l	(A4	h) Mas	onry	y Wall at Ci	<u>rest</u>		,
				A	$\mathbf{A}4_{a}=2$	-			t ≥ 3 m		2.0	
							Wall He	eight	t < 3 m		1.5	
						1	No Mas	onr	y Wall		1.0	$A4_h = 1$
(D) ACTIAL	DEDEC	)DMA	NCE (	4 D)								$A4_h - 1_h$
(B) ACTUAL		JKMA	NCE (	AP)								
(B1) <u>Signs of Di</u> (i) Severe										<u>B1</u> 10		
(ii) Moder										4	B1	1
(iii) Minor	/None									1		
(B2) <u>Instability</u> a	after Slo	pe For	mation	/Treatn	<u>nent</u>							
(i) Massi	ve failu	res (>	500 m <sup>3</sup>	)						<u>B2</u> 10		
	or repe				of distres	SS				5		
(iii) Minor							s of dis	tres	s	2	B2	2
(iv) No fai	lure or	records	of pre	vious m	ninor signs	s of dis	stress			1		

INSTABILITY SCORE (IS)		
$IS_I$ = Instability Score for Sliding and Minor Washout = $AI \times A2 \times B1 \times B2$	$IS_1$	960
$IS_2$ = Instability Score for Liquefaction = $AI \times A3 \times B1 \times B2$	$IS_2$	264
$IS_3$ = Instability Score for Major Washout = $A1 \times A4 \times B1 \times B2$	$IS_3$	10

C <b>O</b> I	NSE(	QUENCE SCORE (CS)			
(C)	FAC	CILITY ABOVE CREST OF FEATURE			
	(i)	Type of crest facility (for roads and footpaths, give also the name) (refer to Table 2.1 of the main text)	Open car park	Facility Group 1 (a)	<i>C1</i>
	(ii)	Facility Group	3	1 (b) 2 (a) 2 (b)	3 2 1
	(iii)	Distance (D) from crest of feature to crest facility (refer to Figure 2.1 of the main text)	1 m	3 4 5	0.25 0.002 0.0002
				CI	0.25
		Vulnerability Factor, C2 (refer to Table 5.1 of the main text)		C2 <sub>1</sub> C2 <sub>2</sub> C2 <sub>3</sub>	0.15 0.15 0.18
D)	FAC	CILITY AT TOE OF FEATURE		I	
	(i)	Type of toe facility (for roads and footpaths, give also the name) (refer to Table 2.1 of the main text)	Densely-used playground	Facility Group 1 (a) 1 (b)	D1 9 3
	(ii)	Facility Group	3	2 (a) 2 (b)	2
	(iii)	Distance ( <i>L</i> ) from toe of feature to toe facility (refer to Figure 2.1 of the main text)	0 m	3 4	0.25
			V III	5	0.0002

<ul> <li>(iv) Shadow angle (ω) from crest of feature to toe facility (refer to Figure 2.1 of the main text)</li> <li>(v) Vulnerability Factor, D2 (refer to Table 5.2 of the main text)</li> </ul>	40 °	D1  D2 <sub>1</sub> D2 <sub>2</sub> D2 <sub>3</sub>	0.25 0.32 0.52 0.315
CONSEQUENCE SCORE (CS)			
$CS_i = (C1 \times C2_i + D1 \times D2_i) \times H$			
Sliding and minor washout failure, $i = 1$			
Liquefaction failure, $i = 2$			
Major washout failure, $i = 3$			
			_
		$CS_1$	1.52
		$CS_2$	2.17
		$CS_3$	1.60

CALCULATED SCORES		
$TOTAL SCORE (TS)$ $TS = \sum_{i=1}^{3} IS_i \times CS_i$	TS	2057.3

# Appendix D

Details of NPRS for Retaining Walls

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## **D.1** Total Score (TS) Computation Sheets for Retaining Walls

FEATURE NO.	SECTION:	O 1-1 (Most Severe Consequence) O 2-2 (Maximum Feature Height)						
(A) INSTABILITY POTENTIAL (IP)								
(A1) Level of Geotechnical Engineering Input  (i) Features with none or little geotechn	<u>AI</u> 10							
(ii) Features with indication of some geo (iii) Features with indication of substantia		3 pput 1 A1						
For retaining walls excluded from ranking	(see Note 7), denote $AI = 0$	AI						
(A2) Geometry (refer to Figure D1)								
(i) Wall Height, $H_w$ Section 1-1 2-2 m m	(ix) Feature Height, $H$ $H = H_s + H_r + H_w$	m						
(ii) Rock Slope Height, $H_r$ m m	(x) Effective Height, $H_e$ $H_e = H_w (1 + 0.35 \tan \beta) + 0.000 \sin \beta$	$-\frac{s}{\gamma_b}$ m						
(iii) Soil Slope Height, $H_s$ m m	where $\gamma_b$ = soil bulk unit we	ight $\frac{kN}{m^3}$						
(iv) Upslope $\circ$ Angle, $\beta$	(xi) $H_e/B_w =$							
(v) Wall Face o Angle, $\theta_w$								
(vi) Surcharge at crest of wall, s kPa kPa								
(vii) Base width, $B_w$								
(viii) Average Wall Face Angle (in case of multiple walls), θ								

Classification (i) $H_e/B_w > 4.2$ (ii) $3.5 < H_e/B_w \le 4.2$ (iii) $2.8 < H_e/B_w \le 3.5$ (iv) $2.0 < H_e/B_w \le 2.8$ (v) $H_e/B_w \le 2.0$				A2 8 6 4 2	A2		
(A3) Wall Type (refer to Figure I  Type of Wall  Random rubble masonry v		hout pointing, ties	or	<i>A3</i>			
<ul><li>Wall composed of lime-stab</li><li>Brick Wall</li><li>Dry packed dressed block/so</li></ul>	horizontal beams)  • Wall composed of lime-stabilised soils  • Brick Wall  • Dry packed dressed block/squared rubble wall without ties  • Any type of masonry wall (except for random rubble walls) with						
<ul> <li>Dry packed dressed block/so</li> <li>Any type of masonry wall concrete horizontal beams</li> </ul>	=		rith	3			
Masonry facing to concrete v     Concrete wall  Other Well Type	A3						
Other Wall Type  (A4) Surface Protection and Surface Drainage							
Surface Protection Surface Drainage	Crest area substantially unprotected	Crest area partially protected	substa	t area intially ected			
Few or no channels above wall crest, and potential for convergent flow of surface water above crest	8	4	2	2			
Few or no channels above wall crest	4	2	1	.5			
Adequate channels	2	1.5		1	A4		

#### (A5) Signs of Seepage and Leaky Water-Carrying Services Water-carrying Presence of potentially leaky services & signs of leakage noted Presence of potentially No potentially leaky services leaky services but no signs of leakage noted Signs of Seepage 8 4 2 Seepage at mid-height or above 4 2 Seepage below mid-height 1.5 2 1.5 1 No signs of seepage A5

(B) A(	TUAL PERFORMANCE (AP)						
	B1) Signs of Distress (i) Severe  B1 10						
(i)	Severe (Advanced stage of severe deformation and/or distress or onset of severe deformation and/or distress)	10					
(ii)	Moderate (Moderate deformation and/or distress)	4					
(iii)	Minor/None (Minimal deformation and distress)	1	B1				
	or a wall of the slenderness ratio, $H_e/B_w \ge 5$ or a dry packed random bble wall with $H_w > 5$ m, accord $BI = 10$						
(B2) <u>Ins</u>	tability after Wall Formation/Treatment	B2					
(i)	Major (full-height failure)	<u>B2</u> 10					
(ii)	Multiple part-height or structural failures, or records of previous severe signs of distress	5					
(iii)	Part-height or structural failures, or records of previous moderate signs of distress	2	B2				
(iv)	No failure nor records of previous signs of distress	1					

( <b>C</b> )	FACILITIES ABOVE CREST	OF FEATURE			
	(i) Type of crest facility (for roads and footpaths, give			Facility Group	C1
	(refer to Table 2.1 of the mai	(refer to Table 2.1 of the main text)		1 (a)	9
				1 (b)	3
	(ii) Facility Group			2 (a)	2
				2 (b)	1
				3	0.25
	(iii) Distance (D) from crest of fe (refer to Figure 2.1 of the ma	•	m	4	0.002
	(Telef to Figure 2.1 of the ma	in text)		5	0.0002

			CI	
(iv	v) Vulnerability Factor, C2 (refer to Table 3.1 of the main text)		C2	
(D) FA	CILITY AT TOE OF FEATURE			
(i)	Type of toe facility (for roads and footpaths, give also the name) (refer to Table 2.1 of the main text)		Facility Group 1 (a)	<i>D1</i> 9
(ii)	Facility Group		1 (b) 2 (a) 2 (b)	3 2 1
(iii	) Shadow angle (a) from crest of feature to toe facility (refer to Figure 2.1 of the main text)	0	3 4 5	0.25 0.002 0.0002
(iv)	Distance ( <i>L</i> ) from toe of feature to toe facility (refer to Figure 2.1 of the main text)	m	D1	
(v)	Vulnerability Factor, D2 (refer to Table 3.2 of the main text)		D2	
CALCUI	LATED SCORES			
	ILITY SCORE (IS) $A2 \times A3 \times A4 \times A5 \times B1 \times B2$		IS	
	NUENCE SCORE (CS) x C2 + D1 x D2] x H		CS	
$\frac{\text{TOTAL S}}{TS = IS \text{ x}}$	SCORE (TS)		TS	

#### D.2 Guidelines on Data Collection and Score Computation for Retaining Walls

#### General

- (1) For composite features, i.e. with more than one type of slope feature, the criteria for computation of the Total Score (*TS*) are presented in Figures 2.3 and 2.4 of the main text.
- (2) If H of Section  $1-1 \ge 75\%$  of H of Section 2-2, consider Section 1-1 (i.e. in terms of most severe consequence) in calculating the scores. Otherwise, both Sections 1-1 and 2-2 (in terms of maximum feature height, H) should be considered.
- (3) Geometric parameters of the feature (e.g.  $H_s$ ,  $H_r$ ,  $H_w$ ,  $\beta$ , and  $\theta_w$ ) (see Figure D1) may be obtained from survey plans and site measurements.
- (4) Detailed physical inspection on the features should be carried out using all available access/route.
- (5) Unless stated otherwise, "distance" refers to horizontal distance and "height" refers to vertical height.
- (6) Details of field mapping and site observation should be recorded using the agreed data collection sheet. Sample data collection sheets for retaining walls are appended for reference. Inspecting engineers may modify the sheets to suit their specific use. Provide photographic records of the overview of the features and facilities affected. The photographic records should also include details of site observation to substantiate the factors adopted in the calculation.

#### Factor A1

- (7) Retaining walls that were processed and accepted by GEO (e.g. retaining walls checked by GEO without outstanding comments, and retaining walls designed by GEO) will not be ranked. Denote these walls with AI = 0. Data on these walls should still be collected.
- (8) The level of geotechnical engineering input should be inferred from databases, files and documentary records kept by GEO and other relevant government departments and organizations, or aerial photographs if necessary.
- (9) Retaining walls with none or little geotechnical engineering input, e.g.
  - pre-1978 walls
  - post-walls formed by unauthorized works
  - post-1978 walls falling outside any engineering project boundary
- (10) Retaining walls with indication of some geotechnical engineering input, e.g.
  - post-1978 walls without GEO checking records but falling within the boundary of engineering projects

- walls assessed as being upto the required safety standard without site specific ground investigation and laboratory testing
- (11) Retaining walls with indication of substantial geotechnical engineering input, e.g.
  - walls checked by GEO but with outstanding comments

#### Factor A2

- (12) A retaining wall is defined as one with an average face angle  $(\theta_w)$  of  $75^\circ$  or more. Where  $\theta_w$  is less than  $75^\circ$ , it would be considered as a rigid surface protection to a slope.
- (13) An assessment of the surcharge (*s*) above the wall crest may be made by reference to Table 16 of the second edition of Geoguide 1 (GEO, 1993).
- (14) In the case of a series of walls retaining a number of platforms, the walls should be considered as a single feature if the average angle ( $\theta$ ) of the line joining the toe of the lowermost wall and the top of the uppermost wall is  $\geq 60^{\circ}$  (Figure D1). If  $\theta \leq 60^{\circ}$ , the individual walls should be considered as separate walls for data collection purposes if each wall is "registrable" based on the SIRST criteria. The criteria for features requiring registration should refer to GEO Circular No. 15 (GEO, 2004).
- (15) The base width of a wall should be determined from the available records as far as possible. In case no record is available, the base width may be inferred from weephole probing. If the base width cannot be determined by the above means, accord the wall slenderness ratio,  $H_e/B_w = 5$ .

#### Factor A3

- (16) Concrete walls sometimes have a decorative masonry facing which can give the impression of being a masonry wall. This type of wall can often be distinguished by the presence of vertical movement joints at a regular spacing, uniformity of the pointing and regular squared-shaped, well dressed blocks. Smaller squared blocks, not necessarily laid in horizontal courses, but arranged to create a regular pattern on the wall face, and often without pointing, have also been used as a decorative facing to concrete walls. Examples of common types of masonry walls and masonry facings are shown in Figures D2 and D3.
- (17) If the wall type is not included in the table, specify the wall type and accord an appropriate weighting by benchmarking with the listed wall type of similar characteristics.

#### Factor A4

(18) Both hard cover and vegetation cover are considered as slope protection. As a general guideline, "substantially protected" refers to more than 75% area covered,

- "partially protected" refers to between 25% and 75% area protected and "substantially unprotected" refers to less than 25% area covered.
- (19) Crest area refers to the area within a horizontal distance of H/2 beyond the crest of the wall.
- (20) Where there is potential for ponding above the wall crest, the score for the next higher category in the surface protection should be adopted.
- (21) In assessing the adequacy of surface drainage provisions, the overall setting including the site topography, catchment area and environmental factors that are liable to give rise to convergent flow of surface water should be considered.
- (22) The potential for convergent flow of surface water above the wall crest should be determined from topographic plan and/or aerial photographs.

## Factor A5

- (23) Assessment of the seepage conditions should be based on site inspection.
- (24) Any water-carrying services that could potentially affect the retaining wall in the event of leakage, typically water-carrying services within *H* from the crest of the retaining wall, should be considered. However, each case should be treated on its merits in determining the extent necessary for the assessment. If proper ducting provisions have been provided, the services may be taken as not "potentially leaky".
- (25) Staining on the wall and erosion features often indicates seepage. When seepage is noted on the wall, the location of the seepage should be marked on plan and section. If the inspection is carried out during the dry season, a conservative assessment of the seepage condition should be made.
- (26) Consideration should also be given to the overall setting of the retaining wall, e.g. whether the retaining wall is at the head of a valley, along the side of a valley or across the nose of a spur, presence of hydrogeological features (e.g. streamcourse) which might contribute water to the retained material, or evidence of a high water table upslope (e.g. an unusually rich vegetation cover).

#### Factors *B1* and *B2*

- (27) Signs of distress are based on site observations, and relevant inspection and maintenance records. The inspecting engineers are required to exercise professional judgement in deciding whether the signs of distress are genuine indication of unsatisfactory performance of the feature. Examples of severe signs of distress are shown in Appendix F of this report.
- (28) Minimal distress refers to wall fabric in good condition; moderate distress refers to the situation where much mortar is missing, or where there is minor dislocation of isolated

- wall blocks; onset of severe distress refers to the situation where some of the wall blocks are missing or dislocated; advanced stage of severe distress refers to the condition where many of the wall blocks are missing or subject to major dislocation. Some guidelines for evaluating the state of wall deformation are given in Table D1.
- (29) Judgment should be made in assessing whether apparent signs of distress (such as cracking) are induced during wall construction or due to inadequate maintenance. In the latter circumstances, although maintenance work may be required, they should not be regarded as signs of distress. In case of doubt, a conservative assessment should be made.
- (30) Instability after treatment accounts for landslide incidents occurred after the wall was formed or substantially modified to its present configuration and upgrading works have not been carried out on the wall subsequent to the incidents.
- (31) Where there are severe signs of distress or documented evidence of continuing hazardous movement, immediate action should be taken.

#### Factors *C* and *D*

(32) Shadow angle ( $\omega$ ) as shown in Figure 2.1 of the main text should be determined by site measurements and/or from survey plans and sections.

#### References

- GEO (1993). *Guide to Retaining Wall Design (Geoguide 1) 2<sup>nd</sup> Edition*. Geotechnical Engineering Office, Hong Kong, 258 p.
- GEO (2004). Registration and Updating of Records of Features (GEO Circular No, 15). Geotechnical Engineering Office, Hong Kong, 20 p.

Table D1 Guidelines for Evaluation of the State of Wall Deformation

Observed State of Wall Deformation	Forward Movement	Bulging
(1) Minimal Deformation	Forward movement of wall as indicated by:  (a) long continuous movement cracks at wall crest sub-parallel to wall, total width at any section < 0.1% of wall height  or  (b) sub-vertical through cracks in return wall of total width at each level < 0.1% h where h is height of measurement point from ground surface level in front of toe	Negligible bulging of wall
(2) Moderate Deformation	Forward movements as (1) except crack width totalling between 0.1% and 0.2% h	Minor bulging of wall face noticeable to naked eye
(3) Onset of Severe Deformation	Forward movements as (1) except crack width totalling between $0.2\%$ and $0.6\%$ $h$	Bulged profile of wall face sufficient to touch a vertical line drawn through wall toe, or maximum bulging of wall approaching or equal to 75 mm
(4) Advanced Stage of Severe Deformation	Forward movements as (1) except crack width totalling to a value $> 0.6\%h$	Bulging as (3) but protruding beyond a vertical line drawn through toe, or maximum bulging of wall > 75 mm

Note:

In using this table, engineering judgment is crucial since different wall types are likely to present different degrees of difficulty in deformation determination. The proposed deformation limits shown in this table shall not be regarded as absolute.

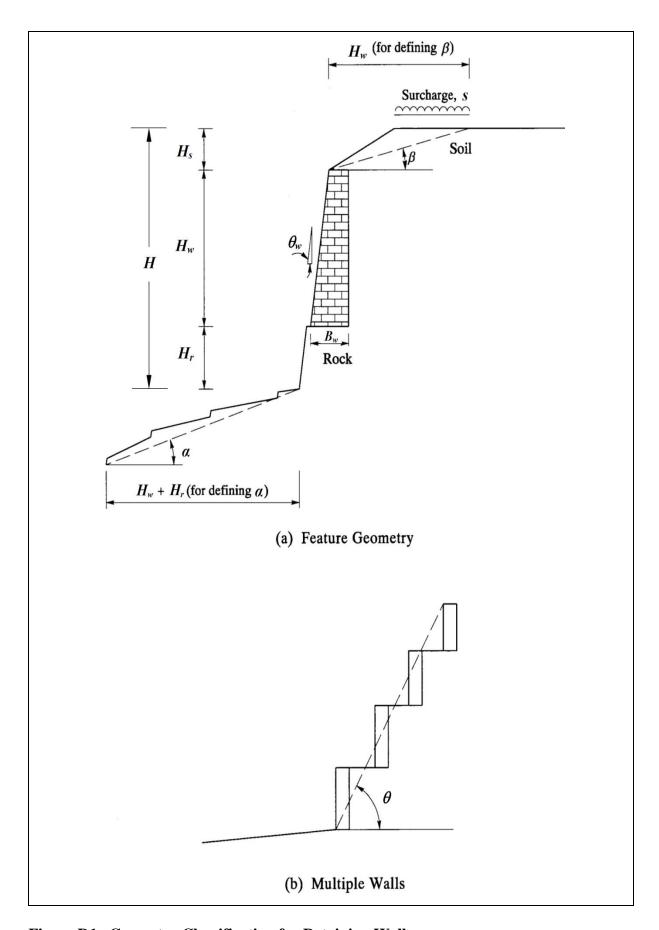


Figure D1 Geometry Classification for Retaining Walls

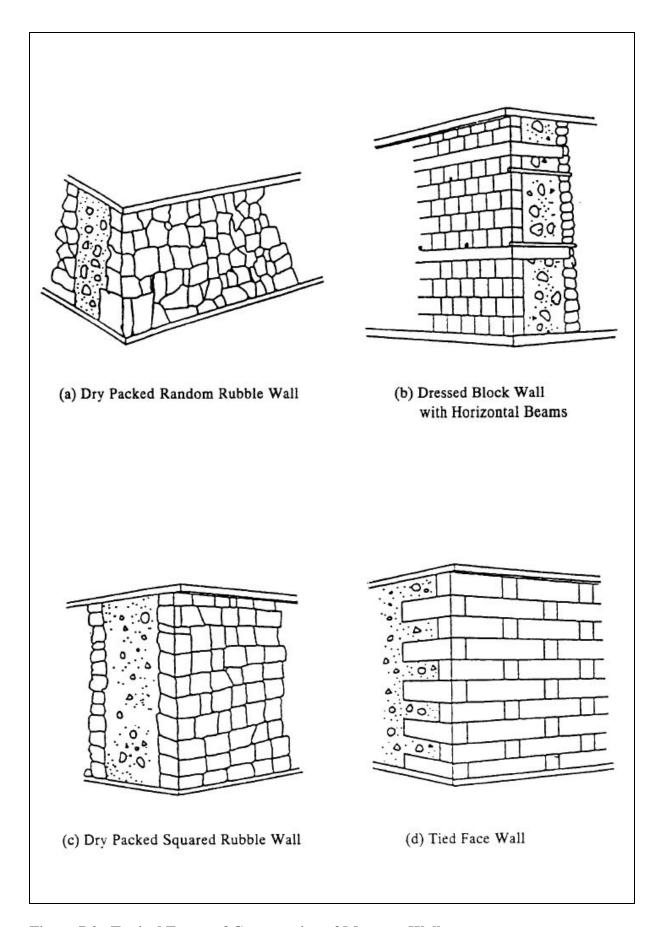


Figure D2 Typical Forms of Construction of Masonry Walls

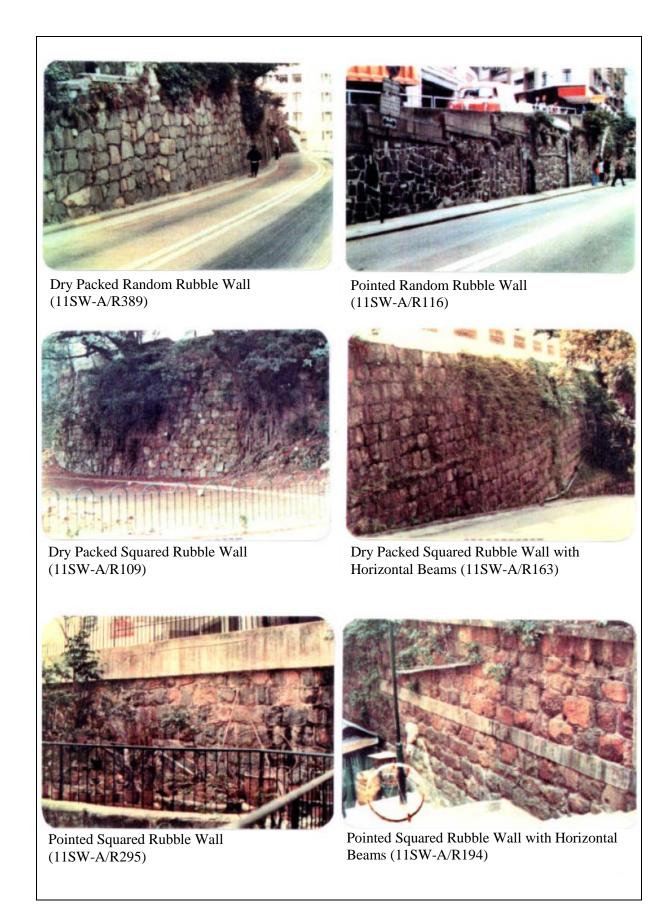


Figure D3 Common Types of Masonry Walls and Masonry Facings (Sheet 1 of 3)

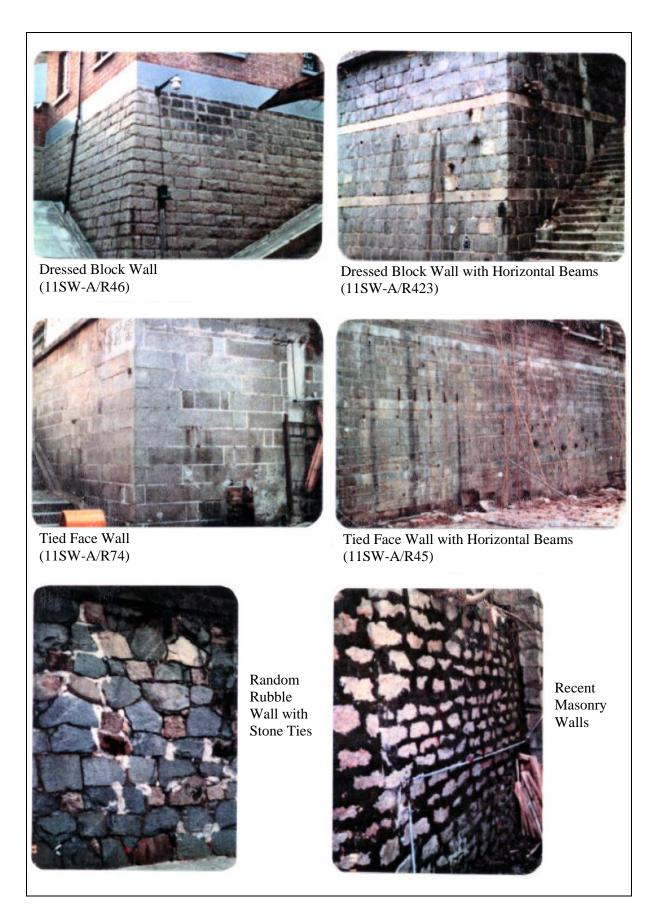


Figure D3 Common Types of Masonry Walls and Masonry Facings (Sheet 2 of 3)



(a) Presence of expansion joints or similar construction joints



(b) Special architectural features, such as masonry blocks with irregular pattern

Figure D3 Common Types of Masonry Walls and Masonry Facings (Sheet 3 of 3)

## **D.3** Sample Data Collection Sheets for Retaining Walls

FEATURE NO. (Page 1 of )						
SECTION: O	1-1 (Most S	Severe Conse	quence)	O 2-2 (	Maximum Feat	ure Height)
Check if $H_1 \ge 75\%$ x $H_2$ .	If yes, consid	der Section 1	-1 only; If no,	consider both Sections	s 1-1 and 2-2	
Geometry (refer to Figure	D1)					
	Section 1-1	2-2			Section 1-1	2-2
(i) Wall Height, $H_w$	m	m	(ix) Feature I $H = H_s +$	-		m
(ii) Rock Slope Height, $H_r$	m	m	(x) Effective $H_e = H_w$ (	e Height, $H_e$ $(1 + 0.35 \tan \beta) + \frac{s}{\gamma_b}$		m
(iii) Soil Slope Height, $H_s$	m	m	where $\gamma_b =$	soil bulk unit weight		$\frac{kN}{m^3}$
(iv) Upslope Angle, $\beta$	0	О				
(v) Wall Face Angle, $\theta_w$	0	0	(xi) $H_e/B_w =$			
(vi) Surcharge at Crest of Wall, s	kPa	kPa	<u>Notes</u>			
(vii) Base Width, $B_w$			If $\theta_{\rm w}$ < 75 °, protection to	the wall should be con a slope. The feature e in computation of the	e should be treat	
(viii) Average Wall Face Angle (in case of multiple walls), $\theta$	0	0	feature. Ot	ne walls should be con therwise, individual wa they are registrable.		
Do the dimensions of indiv of the main text?	ridual feature ty	pes satisfy the	e requirement o	of separate Total Score	as shown in Figu	res 2.3 & 2.4
• Yes  If yes, number of data co	o l		this section :			
Affected Facilities (refe	er to Figure 2.	1 and Table 2	.1 of the main	text)		
Section 1-1	Fa	acility Type		Facility Group	Proxim	nity
Toe					L=	m
100					ω=	O
Crest					D =	m
Section 2-2	Fa	acility Type		Facility Group	Proxin	nity
Toe					L = ω=	m o
Crest					D =	m

FEATURE NO.	EATURE NO. (Page 2 of )						
PLAN AND CROS	SS-SEC	ΓΙΟΝ					
SECTION:	0	1-1 (Most Severe Consequen	nce)	0	2-2 (Maximum Feature Height)		
Notes: PLAN (1:1000)  1. Feature boundary (SIS) a 2. Section Mark 3. Photo Location and Dire 4. Signs of distress, if any 5. Signs of seepage, if any 6. Engineering measures (e	ection	d Feature Boundary (if applicable)	CROSS-SECTIONS 1. Fully dimensioned 2. Existing engineering	; measures	s. (e.g. thickening & skin walls)		

FEATURE NO.	(Page 3 of )
WALL CHARACTERISTICS	SITE OBSERVATIONS/FINDINGS
Wall Type	<ul> <li>Random rubble masonry wall</li> <li>Brickwall</li> <li>Wall composed of lime stabilized soil</li> <li>Dry-packed dressed block or squared rubble wall         <ul> <li>with ties</li> <li>without ties</li> </ul> </li> <li>Masonry wall other than random rubble wall         <ul> <li>with horizontal beam(s) made of concrete</li> <li>with horizontal beams(s) made of lime-soil or brick</li> <li>without horizontal beam(s)</li> </ul> </li> <li>Concrete wall (with or without masonry facing)</li> <li>Others:</li></ul>
Base Width, $B_W$	Base Width mm as determined from  O Documentary records (Thickness Gauging/EI/MM/As-built drawings)  Weephole Probing (Provide field weephole probing record on Page 5)  Others:
Surface Protection	Surface cover with  Vegetation
	Location Size (mm) Spacing (m) Type (e.g. U-channel, Step channel, downpipes or ditch) (Y/N) Remarks

## 

FEATURE NO.				(Page 4 of )		
WALL CHARACTERISTICS	SITE OBSERVATIONS/FINDINGS					
	Signs of Seepage?		o Yes	o No		
	If Yes, provide the following	details	Condition of seepag	ge		
Signs of Seepage	Seepage Location  At or above mid-height	Copious	Trickling/damp	Stain		
	Below mid-height  Others:  Indicate seepage location on	nlan and section				
Water-carrying Services	Indication of presence of underground water-carrying services above or behind the wall:  O Valve(s) of water main within crest area/on the wall  Manhole cover(s) within crest area/on the wall  Others:  Signs of leakage?  O Yes  O No  If Yes, indicate location and condition of leakage					
Signs of Distress  (Provide photographic records of signs of distress and indicate location & extent on plan & cross-sections)	<ul> <li>No indication of any signs</li> <li>Reported signs of distress of the National Deformation of the Wall</li> <li>Long continuous crace Crack width</li> <li>Sub-vertical through Crack width</li> <li>Bulging of wall face Horizontal distance I and the wall toe =</li> <li>Fabric condition of rubble of General intact without the Company of Missing mortar/point of Missing mortar/point of Minor dislocation of the Some blocks missing</li> <li>Where severe signs of follow-up action should be made cracking) are induced during the latter circumstances</li> </ul>	ck at wall crest summ, equivalent crack in return wall crest in measured a create in measured a create in measured a create in signs of distresuring missing ing at several locks or dislocated distress or haza e taken immediate in assessing whing wall construction.	ub-parallel to wall; to % of wall vall at m above toe ical line from the pe iss cations ardous movement is tely. hether apparent signs action or due to inade	noted, appropriate of distress (such as equate maintenance.		

FEATURE NO.		(Page 5 of )
WALL CHARACTERISTICS	SITE OBSERVATIONS/FINDINGS	
Instability after Wall Formation/Treatment  (Provide photographic records of the inferred failure scar and indicate location on plan & cross-sections)	<ul> <li>No indication of any failure occurred after formation or treatment</li> <li>Reported failure of the wall</li> <li>Possible failure scar observed at of the wall</li> <li>Estimated failure volume = m³</li> <li>Debris observed on site/Other observations:</li> </ul>	
OTHER OBSERVATIONS/REI	MARKS	
INSPECTION DATE:	/ / (dd/mm/yyyy) BY:	

FEATURE NO.	(Page 6 of	)
PHOTOGRAPHIC RECORDS		
[Caption]		
PHOTOGRAPHIC RECORDS		
[Caption]		
Notes: (1) Indicate photograph vantage points on plan (2) Add more pages for additional photographic records/sketches		

## **D.4** Worked Example (Data Collection Sheets)

Section 2 - 2

Toe

Crest

FE	ATURE NO. "Wo	orked Exam	ple 4''				(P	Page 1 of 7)
SE	CTION:	1-1 (Most S	Severe Conse	quence)	O 2-2 (	Maximum l	Feature	Height)
Che	eck if $H_1 \ge 75\% \times H_2$ .	. If yes, consi	der Section 1	-1 only; If no,	consider both Section	s 1-1 and 2-	2	
Geo	ometry (refer to Figur							
		Section 1-1	2-2			Section 1-1		2-2
(i)	Wall Height, $H_w$	8.3 m	— m	(ix) Feature $H = H_s + \frac{1}{2}$	Height, $H$ $H_r + H_w$	8.3 m		— m
(ii)	Rock Slope Height $H_r$	m	— m	(x) Effective $H_e = H_w$	e Height, $H_e$ $(1 + 0.35 \tan \beta) + \frac{s}{\gamma_b}$	8.8 m		— m
(iii)	Soil Slope Height, $H_s$	— m	— m	where $\gamma_b$	= soil bulk unit weight	20	$0\frac{\mathrm{kN}}{\mathrm{m}^3}$	
(iv)	Upslope Angle, $\beta$	<b>0</b> °	0				<b>-</b> ,	
(v)	Wall Face Angle, $\theta_w$	85 °	0	(xi) $H_e/B_w =$		8.8		_
(vi)	Surcharge at Crest of Wall, s	10 kPa	— kPa		since $H_{e^t}$	$/B_w > 5$ , ac	cord	BI = 10
(vii	) Base Width, $B_w$	1.0 m	_	protection to	the wall should be contained a slope. The feature in computation of the	e should be		
(vii	ii) Average Wall Face Angle (in case of multiple walls), $\theta$	e o	0	feature. O	ne walls should be con therwise, individual w they are registrable.		_	ered
	the dimensions of indi he main text?	ividual feature ty	ypes satisfy th	e requirement o	of separate Total Score	as shown in	Figures	2.3 & 2.4
If	○ Yes   No  If yes, number of data collection sheets required for this section :							
<u> </u>	Affected Facilities (re-	fer to Figure 2.	1 and Table 2	2.1 of the main	text)			
	Section 1 - 1			Facility Group		oximity	,	
	Toe	U	e, licensed uatter area		1(b)		0 m 85 °	
	Crest	Road with	low traffic	density	4	D=	0	m

Facility Type

Facility Group

Proximity

m o

m

L =

 $\omega = D = D$ 

# FEATURE NO. "Worked Example 4" (Page 2 of 7) PLAN AND CROSS-SECTION **SECTION:** 1-1 (Most Severe Consequence) 2-2 (Maximum Feature Height) 0 3 m long and 3 mm wide vertical crack at 1.3 m above Localized missing pointings Single storey garage **PLAN** (Not to scale) Notes: PLAN (1:1000) 1. Feature boundary (SIS) and Revised Feature Boundary (if applicable) 2. Section Mark 3. Photo Location and Direction

- 4. Signs of distress, if any
- 5. Signs of seepage, if any6. Engineering measures (e.g. thickening & skin walls)

- CROSS-SECTIONS

  1. Fully dimensioned
  2. Existing engineering measures. (e.g. thickening & skin walls)

# FEATURE NO. "Worked Example 4" (Page 3 of 7) PLAN AND CROSS-SECTION **SECTION:** 1-1 (Most Severe Consequence) 0 2-2 (Maximum Feature Height) Worked Road with Example 4 low traffic density Masonry wall with concrete beams $\theta_w = 85^{\circ}$ Single H storey 3.3 garage $\omega = 85^{\circ}$

Note: No reinforcement or structural support observed on site

## Section 1-1 (Not to scale)

- 1. Feature boundary (SIS) and Revised Feature Boundary (if applicable)
- 2. Section Mark

- Section Mark
   Photo Location and Direction
   Signs of distress, if any
   Signs of seepage, if any
   Engineering measures (e.g. thickening & skin walls)

#### CROSS-SECTIONS

- 1. Fully dimensioned
- 2. Existing engineering measures. (e.g. thickening & skin walls)

 $B_{w} = 1 \text{ m}$  (by weephole probing)

FEATURE NO. "Worke	ed Example 4"		(Page 4 of 7)		
WALL CHARACTERISTICS	SITE OBSERVATIONS/FINDINGS				
Wall Type	<ul> <li>Random rubble masonry wall</li> <li>Brickwall</li> <li>Wall composed of lime stabilized soil</li> <li>Dry-packed dressed block or squared rubble wall</li> <li>with ties</li> <li>without ties</li> <li>Masonry wall other than random rubble wall</li> <li>with horizontal beam(s) made of concret</li> <li>with horizontal beams(s) made of lime-s</li> <li>without horizontal beam(s)</li> <li>Concrete wall (with or without masonry facing)</li> <li>Others:</li> </ul>	oil or brick			
Base Width, $B_w$	Base Width mm as determined from  O Documentary records (Thickness Gauging/EI/MM/As-built drawings)  ✓ Weephole Probing (Provide field weephole probing record on Page 6)  O Others:				
Surface Protection	Surface cover with  ○ Vegetation				
	Location Size (mm) Spacing (m) Type (e.g. U-channe step channel, downpipes or ditch)  Crest	Capacity	Remarks		
Surface Drainage Provision	Berm On Slope Toe  O Potential surface runoff converge onto the crest area	due to topogra	bhy (observed		
	or inferred from topographic plan or aerial photos)  ○ Feature located on a drainage line/zone of depression  ○ Inadequate surface drainage evident by surface erosi  ✓ Other observations/records : No surface drainage	on or erosion gul	-		

FEATURE NO. "Worked Example 4"				(Page 5 of 7 )	
WALL CHARACTERISTICS	SITE OBSERVATIONS/FINDINGS				
Signs of Seepage	Signs of Seepage?  If Yes, provide the following details  Seepage Location		○ Yes   ✓ No  Condition of seepage		
	At or above mid-height  Below mid-height  Others:  Indicate seepage location on p			Stain	
Water-carrying Services	Indication of presence of underground water-carrying services above or behind the wall:  Valve(s) of water main within crest area/on the wall  Manhole cover(s) within crest area/on the wall  Others:  Signs of leakage?  Yes  No  If Yes, indicate location and condition of leakage				
Signs of Distress (Provide photographic records of signs of distress and indicate location & extent on plan & cross-sections)	<ul> <li>○ No indication of any signs of distress</li> <li>○ Reported signs of distress during inspection or in maintenance records</li> <li>✓ Observed signs of distress (please tick)</li> <li>Deformation of the Wall</li> <li>○ Long continuous crack at wall crest sub-parallel to wall;         Crack width mm, equivalent to % of wall height</li> <li>✓ Sub-vertical through crack in return wall         Crack width3 mm measured at0.5 m above toe</li> <li>○ Bulging of wall face         Horizontal distance between the vertical line from the peak of bulged profile and the wall toe = mm</li> <li>Fabric condition of rubble/masonry wall</li> <li>○ General intact without signs of distress</li> <li>○ Localised mortar/pointing missing</li> <li>✓ Missing mortar/pointing at several locations</li> <li>○ Minor dislocation of isolated blocks</li> <li>○ Some blocks missing or dislocated</li> <li>Where severe signs of distress or hazardous movement is noted, appropriate follow-up action should be taken immediately.</li> <li>Judgment should be made in assessing whether apparent signs of distress (such as cracking) are induced during wall construction or due to inadequate maintenance. In the latter circumstances, they should not be regarded as signs of distress.</li> </ul>				

#### FEATURE NO. "Worked Example 4" (Page 6 of 7) WALL SITE OBSERVATIONS/FINDINGS **CHARACTERISTICS** ✓ No indication of any failure occurred after formation or treatment Instability after Wall Reported failure \_\_\_ Formation/Treatment o Possible failure scar observed at \_\_\_\_\_\_ of the wall (Provide photographic Estimated failure volume = \_\_\_\_\_ m<sup>3</sup> records of the inferred failure scar and indicate o Debris observed on site/Other observations: location on plan & cross-sections)

#### OTHER OBSERVATIONS/REMARKS

- 1. According to SIFT Report, this retaining wall was formed pre-1978.
- 2. The base width of the wall,  $B_w = 1$  m was estimated by weephole probing on site. Three weepholes were probed (Length = 0.9 m, 0.95 m, and 1.1 m) and the wall face angle was considered in the estimation of the base width.

INSPECTION DATE: 24 / 01 / 2009 (dd/mm/yyyy) BY: PAJ

### FEATURE NO. "Worked Example 4"

(Page 7 of 7)

### PHOTOGRAPHIC RECORDS



V1 General View of the Retaining Wall

### PHOTOGRAPHIC RECORDS



V2 Crack and Missing Pointings

### Notes:

- Indicate photograph vantage points on plan
   Add more pages for additional photographic records/sketches

## **D.5** Worked Example (TS Computation Sheets)

FEATURE NO. "Worked Example 4"				SECTION:	<b>6</b>		Severe Consequence) mum Feature Height)
(A) INSTABILIT	Y POTENT	IAL (IP)					
<ul><li>(ii) Features v</li><li>(iii) Features v</li></ul>	vith none or li	ttle geotech	nical engine eotechnical o	eering input engineering input nical engineering in $AI = 0$	input	<u>AI</u> 10 3	A1 10
(A2) Geometry (ref	er to Figure D	<b>D</b> 1)					
(i) Wall Height, $H_w$	Section 1-1  8.3 m	2-2 — m		re Height, $H$ $I_s + H_r + H_w$		8.3 m	
(ii) Rock Slope Height, $H_r$	0 m	— m		tive Height, $H_e$ $H_w (1 + 0.35 \tan \beta)$	$+\frac{s}{\gamma_b}$	8.8 m	
(iii) Soil Slope Height, $H_s$	0 m	— m	where $\gamma_b$	= soil bulk unit w	eight	$20\frac{kN}{m^3}$	
(iv) Upslope Angle, $\beta$	0 °	0	(xi) $H_e/B$	$B_w =$		8.8	
(v) Wall Face Angle, $\theta_w$	85 °	0					
(vi) Surcharge at crest of wall, s	10 kPa	— kPa					
(vii) Base width, $B_w$	1 m	— m					
(viii) Average Wall Face Angle (in case of multiple walls), $\theta$	0	0					

					1	1
Classification (i) $H_e/B_w > 4.2$ (ii) $3.5 < H_e/B_w \le 4.2$ (iii) $2.8 < H_e/B_w \le 3.5$ (iv) $2.0 < H_e/B_w \le 2.8$ (v) $H_e/B_w \le 2.0$				A2 8 6 4 2	A2	8
(A3) <u>Wall Type</u> (refer to Figure 1	D2)					
Type of Wall			A3			
Random rubble masonry v horizontal beams)	wall (with or wit	hout pointing, ties	or 8			
<ul> <li>Wall composed of lime-stab</li> <li>Brick Wall</li> <li>Dry packed dressed block/sc</li> <li>Any type of masonry wall horizontal beams made of line</li> </ul>						
<ul> <li>Dry packed dressed block/so</li> <li>Any type of masonry wall concrete horizontal beams</li> </ul>			vith 3			
Masonry facing to concrete v     Concrete wall	wall		1		A3	3
Other Wall Type						
(A4) Surface Protection and Surf	ace Drainage					
Surface Protection Surface Drainage	Crest area substantially unprotected	Crest area partially protected	Crest area substantially protected			
Few or no channels above wall crest, and potential for convergent flow of surface water above crest	8	4	2			
Few or no channels above wall crest	4	2	1.5			
Adequate channels	2	1.5	1		A4	1.5

### (A5) Signs of Seepage and Leaky Water-Carrying Services

	Presence of potentially leaky services & signs of leakage noted	Presence of potentially leaky services but no signs of leakage noted	No potentially leaky services
Seepage at mid-height or above	8	4	2
Seepage below mid-height	4	2	1.5
No signs of seepage	2	1.5	1

A5

1.5

<b>(B)</b>	ACTUAL PERFORMANCE (AP)		
(B1)	Signs of Distress	<i>B1</i>	
	<ul> <li>(i) Severe         (Advanced stage of severe deformation and/or distress or onset of severe deformation and/or distress)     </li> </ul>	<u>B1</u> 10	
	(ii) Moderate (Moderate deformation and/or distress)	4	
	(iii) Minor/None (Minimal deformation and distress)	1	B1 10
	For a wall of the slenderness ratio, $H_e/B_w \ge 5$ or a dry packed random rubble wall with $H_w > 5$ m, accord $B1 = 10$		
(B2)	Instability after Slope Formation/Treatment	B2	
	(i) Major (full-height failure)	<u>B2</u> 10	
	(ii) Multiple part-height or structural failures, or records of previous severe signs of distress	5	
	(iii) Part-height or structural failures, or records of previous moderate signs of distress	2	B2 <b>1</b>
	(iv) No failure nor records of previous signs of distress	1	

### **(C)** FACILITIES ABOVE CREST OF FEATURE Facility (i) Type of crest facility Road/footpath C1(for roads and footpaths, give also the name) Group with low traffic (refer to Table 2.1 of the main text) density 1 (a) 9 1 (b) 3 (ii) Facility Group 2 (a) 2 4 2 (b) 1 0.25 3 (iii) Distance (D) from crest of feature to crest facility 4 0.002 (refer to Figure 2.1 of the main text) 0 m0.0002 5

(iv) Vulnerability Factor, C2 (refer to Table 3.1 of the main text)		C1 C2	0.002
(D) FACILITY AT TOE OF FEATURE		-	
(i) Type of toe facility (for roads and footpaths, give also the name) (refer to Table 2.1 of the main text)	Cottage, licensed and squatter area	Facility Group 1 (a)	<i>D1</i> 9
(ii) Facility Group	1(b)	1 (b) 2 (a) 2 (b)	3 2 1
(iii) Shadow angle (ω) from crest of feature to toe facility (refer to Figure 2.1 of the main text)	85°	3 4 5	0.25 0.002 0.0002
(iv) Distance (L) from toe of feature to toe facility (refer to Figure 2.1 of the main text)	0 m	D1	3
(v) Vulnerability Factor, D2 (refer to Table 3.2 of the main text)		D2 [	0.15
CALCULATED SCORES			
INSTABILITY SCORE (IS) $IS = A1 \times A2 \times A3 \times A4 \times A5 \times B1 \times B2$		IS	5400
$ \underline{CONSEQUENCE SCORE (CS)} $ $ CS = [C1 \times C2 + D1 \times D2] \times H $		CS	3.74
$ \frac{\text{TOTAL SCORE}(TS)}{TS = IS \times CS} $		TS	20172.4

## Appendix E

Combined Ranking Methodology

## Contents

		Page No.
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E.6	Worked Example (RS Computation)	172

### E.1 Combined Ranking Methodology

The Ranking Score (RS) for a man-made slope feature is determined by assigning a proportion of the total risk to a slope feature of a particular type according to the ratio of the Total Score (TS) to the summation of TS ( $\Sigma TS$ ) of that feature type. It is assumed that the TS of each feature type is linearly related to the relative risk. A constant of  $10^5$  is applied to the computation of RS to make its value larger for easy reference.

The equation is as follows:

$$RS = \frac{TS}{\Sigma TS} \times \frac{Proportion \ of \ Total \ Risk \ for}{a \ Particular \ Feature \ Type} \times 10^{5} \dots (E.1)$$

According to an updated assessment of landslide risk posed by man-made slope features (Cheng & Ko, 2008), the proportions of the total risk associated with soil cut slopes, rock cut slopes, fill slopes and retaining walls are 66%, 10%, 11% and 13% respectively.

A combined ranking involving about 16,600 soil cut slopes, 1,600 rock cut slopes, 6,400 fill slopes and 4,300 retaining walls has been carried out by the GEO. The TS, and hence  $\Sigma TS$  of the individual feature types, were determined on the basis of available data in 2008, using default values where necessary.

Based on the findings of the above mentioned risk assessment and combined ranking, the respective proportion of total risk and  $\Sigma TS$  for each feature type have been substituted in the equation above to give the following equations for the computation of RS:

For soil cut slope  $RS = 0.063 \times TS$  (individual slope feature) For rock cut slope  $RS = 0.022 \times TS$  (individual slope feature) For fill slope  $RS = 0.006 \times TS$  (individual slope feature) For retaining wall  $RS = 0.027 \times TS$  (individual slope feature)

### References

Cheng, P.F.K. & Ko, F.W.Y. (2008). An Updated Assessment of Landslide Risk Posed by Man-made Slopes and Natural Hillsides in Hong Kong (SPR 7/2008). Geotechnical Engineering Office, Hong Kong, 44 p.

## **E.2** Worked Example (Data Collection Sheets - Soil Cut Portion)

FEATURE NO. "Worked Example 5" (Page 1 of 6)							
<b>SECTION:</b> Check if $H_1 \ge 75\%$ x		vere Consequence ler Section 1-1 o		O 2-2 consider both Section	(Maximum Fea	<del>-</del> .	
Geometry (refer to Fig	gure A1)						
	Section 1-1	2-2			Section 1-1	2-2	
Soil Slope Height,	<i>H<sub>s</sub></i> 14 m	— m	Feature He $H = H_s + H$	eight, $H_r + H_{cw} + H_{tw}$	17 m	m	
Rock Slope Height	$H_r$ — m	— m	$H_w = H_{cw} +$	- H <sub>tw</sub>	3 m	— m	
Crest Wall Height, $H_{cw}$	— m	— m	$H_c = H_s + 1$	$H_r$	14 m	_ m	
Toe Wall Height, H	$H_{tw}$ 3 m	— m	$H_o = H_s + $	$H_{cw}\left(+Hr'\right)^{\#}$	14 m	— m	
Upslope Angle, $\beta$	0	0		d include the portion re a realistic slip sur			
Surcharge above the Slope Crest, s	e 10 kPa	— kPa	$H_r$ '		m	m	
Soil Slope Angle,	θ <sub>s</sub> 45°	0	Effective H $H_e = H_o (1 - \frac{1}{2})$	eight, $H_e$ + 0.35 tan $\beta$ ) + $\frac{s}{\gamma_b}$	14.5 m	— m	
Average Slope Ang $\theta$	gle, 45°	0					
Downslope Gradie $\alpha$	ent, o	0	where $\gamma_b$ = soil bulk unit weight $20$			$20\frac{\mathrm{kN}}{\mathrm{m}^3}$	
Do the dimensions of i main text?	ndividual feature ty	pes satisfy the re	quirement of	f separate Total Scor	e as shown in I	Figure 2.3 of the	
<b>√</b> Yes	o No If	f yes, number of	data collect	ion sheets required	for this sectio	on: 2	
Affected Facilities	(refer to Figure 2.1	and Table 2.1)					
Section 1-1	Facility Type (fo	r roads, please g	give name)	Facility Group	Proximity		
Toe	Densely-	Densely-used open area		3		0 m 49°	
Crest	Road with	low traffic de	ensity	4	D =	<b>2</b> m	
Section 2-2	Facility Type (fo	r roads, please g	give name)	Facility Group	Pro	oximity	
Toe		_		_	L = ω=	— m	
Const							

# FEATURE NO. "Worked Example 5" (Page 2 of 6) PLAN AND CROSS-SECTION **SECTION:** 1-1 (Most Severe Consequence) 0 2-2 (Maximum Feature Height) (1)220 UC Crack of slope cover due to tree growth 220 UC Possible failure scar <u>Plan</u> (Not to scale) **CROSS-SECTIONS** Fully dimensioned Engineering measures (e.g. soil nails, shotcrete & buttress) Feature boundary (SIS) and revised feature boundary (if applicable) Section mark Photograph location and direction Signs of distress, if any Signs of seepage, if any Engineering measures (e.g. soil nails, shotcrete & buttress)

### FEATURE NO. "Worked Example 5"

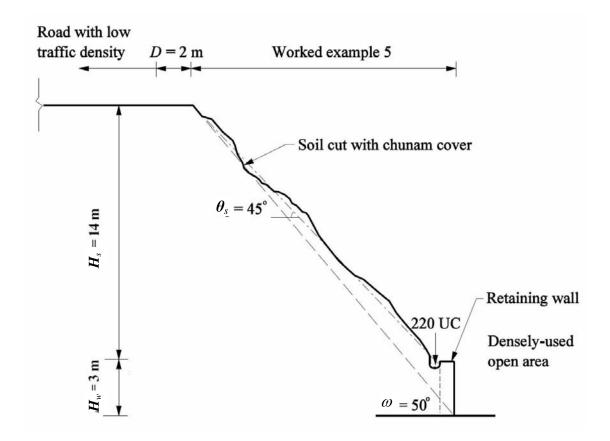
(Page 3 of 6)

### PLAN AND CROSS-SECTION

**SECTION:** 

1-1 (Most Severe Consequence)

0 2-2 (Maximum Feature Height)



Note: No reinforcement or structural support observed on site

### **Section 1-1** (Not to scale)

- Feature boundary (SIS) and revised feature boundary (if applicable)
- Section mark
  Photograph location and direction
  Signs of distress, if any
  Signs of seepage, if any

- Engineering measures (e.g. soil nails, shotcrete & buttress)

### CROSS-SECTIONS

- 1. Fully dimensioned
- 2. Engineering measures (e.g. soil nails, shotcrete & buttress)

FEATURE NO. "Work	ed Example	e 5''					(Page 4 of 6)
SLOPE CHARACTERISTICS			SITE OB	SERVATIONS/I	FINDIN	GS	
Slope Protection	Surface cover with  Vegetation 5 % (including grass/shrubs/trees)  Hard cover 95 % (including concrete/chunam)  Bare surface %  Others %  Substantially protected (> 75%)  Partially protected (25% - 75%)  Substantially unprotected (< 25%)  Zone(s) of depression or potential ponding exist within the crest area H/2  Yes No  If yes, mark the extent of depression or ponding zones on plan and adopt the score of the next higher category in slope protection						
	Location	Size (mm)	Spacing (m)	Type (e.g. U-ch step channe downpipes or o	el,	Adequate Capacity (Y/N)	Remarks
	Crest			_			_
	Berm			<u> </u>		<b>—</b>	— T ! J
Surface Drainage Provision	On Slope Toe	220 220	<u> </u>	Step-chan U-chann	<u>nei</u> el	Y	Lined Lined
	<ul><li>Slope lo</li><li>Inadequal</li></ul>	cated on a ate surface	drainage lin drainage ev	n or aerial photos e/zone of depress ident by surface of	ion erosion	_	lly, etc.
Hydrogeological Settings	Signs of Seep If Yes, prov		ring details	0	Yes	<b>√</b> N	0
(Duovido mhotoguanhio	Saar	age Locat	tion	(	Conditio	n of seepage	
(Provide photographic records of signs of seepage	Sec <sub>1</sub>	age Local	.1011	Copious	Trickling/damp		Stain
and indicate location & extent on plan &	At or above		nt				
cross-sections)	Below mid-l	height					
	o Other ob	servations	s/records:				
Geological Features  (Provide photographic records of the site observations)	<ul> <li>No poter</li> <li>Possible</li> <li>Shear su</li> <li>Clay or s</li> <li>Slickens</li> <li>Disconti</li> <li>Significa</li> </ul>	relict failurfaces/zonsilt filled disconuities head the district head the disconuities head the disconuities head dykes /	rse geologica ure (concave de discontinuities entinuities avily coated nised granite	site observations Il features observe shaped profile) es with dark minera e or volcanics layers within vo	ed or rec	corded	(please tick) :

FEATURE NO. "Worke	d Example 5" (Page 5 of 6)
SLOPE CHARACTERISTICS	SITE OBSERVATIONS/FINDINGS
	<ul> <li>No indication of any signs of distress</li> <li>Reported signs of distress in inspection or maintenance records</li> </ul>
Signs of Distress  (Provide photographic records of signs of distress and indicate location & extent on plan & cross-sections)	<ul> <li>✓ Observed signs of distress (please tick)         <ul> <li>Large tension cracks behind crest (approx mm wide)</li> <li>Significant distortion/damage of channels and berms</li> <li>Severe cracking and bulging of hard surfacing</li> <li>Subsidence inside crest area or on slope surface</li> <li>Extensive cracking of slope cover</li> <li>Isolated minor cracking of slope cover/Isolated cracking of channels</li> <li>Others:</li> </ul> </li> <li>Where severe signs of distress or hazardous movement is noted, appropriate follow-up action should be taken immediately.</li> <li>Judgment should be made in assessing whether cracked slope cover, damaged channels etc. are due to inadequate maintenance, if so, they should not be regarded as signs of distress.</li> </ul>
Instability after Slope Formation/Treatment  (Provide photographic records of the inferred failure scar and indicate	<ul> <li>No indication of any failure occurred after formation or treatment</li> <li>Reported failure</li></ul>
location on plan & cross-sections)	
According to the SIFT	EMARKS  Report, the feature was formed pre-1963.
INSPECTION DATE:	02 / 06 / 2009 (dd/mm/yyyy) BY: <b>PAJ</b>

### FEATURE NO. "Worked Example 5"

(Page 6 of 6)

### PHOTOGRAPHIC RECORDS



V1 General View of the Feature Comprising Soil Cut Slope and Retaining Wall

### Notes:

- Indicate photograph vantage points on plan
   Add more pages for additional photographic records/sketches

## **E.3** Worked Example (Data Collection Sheets - Retaining Wall Portion)

FE.	FEATURE NO. "Worked Example 5" (Page 1 of 6)							
SE	CTION: Ø	1-1 (Most S	Severe Conse	quence)	O 2-2 (	Maximum Fe	ature Hei	ght)
Che	eck if $H_1 \ge 75\%$ x $H_2$ .	If yes, consid	der Section 1	-1 only; If no, o	consider both Sections	s 1-1 and 2-2		
Geo	ometry (refer to Figure	e D1)						
		Section 1-1	2-2	_		Section 1-1	2-2	2
(i)	Wall Height, $H_w$	3 m	— m	(ix) Feature H $H = H_s + \frac{1}{2}$	•	17 m		m
				(x) Effective	Height. $H_a$			
(ii)	Rock Slope Height, $H_r$	' m	— m	, ,	$(1+0.35\tan\beta) + \frac{s}{\gamma_b}$	4.55 m	_	m
(iii)	) Soil Slope Height, $H_s$	14 m	— m	where $\gamma_b = s$	soil bulk unit weight	20	$\frac{kN}{m^3}$	
(iv)	Upslope Angle, $\beta$	45 °	0					
(v)	Wall Face Angle, $\theta_{\scriptscriptstyle W}$	90 °	0	$(xi) H_e/B_w =$		5*		
(vi)	Surcharge at Crest of Wall, s	10 kPa	* Since $B_w$ cannot be determined from documentary record or probing, accord $H_e/B_w = 5$ Notes					
(vii	i) Base Width, $B_w$	Unknown	_	If $\theta_w < 75^{\circ}$ , to protection to	the wall should be con a slope. The feature computation of the NP	e should be tre		
(vii	ii) Average Wall Face Angle (in case of multiple walls), $\theta$	0	0		e walls should be cons ndividual wall should strable.			
	the dimensions of indiv he main text?	vidual feature ty	pes satisfy th	e requirement o	f separate Total Score a	as shown in Fig	gures 2.3	& 2.4
	<b>√</b> Yes	0 1	No					
If y	res, number of data col	llection sheets	required for	this section :	2			
	Affected Facilities (re	efer to Figure 2	.1 and Table	2.1 of the mair	ı text)			
	Section 1 - 1	F	Facility Type		Facility Group	Prox	ximity	
	Toe		-used oper		3	$\omega = 4$	0 m 49 °	
	Crest	Road with	low traffic	c density	4	D = 1	16 I	m
	Section 2 - 2	F	Facility Type		Facility Group	Prox	ximity	
	Toe		_			$L =  \omega = -$	— 1 —	m o
	Crest				_	D = -		m

# FEATURE NO. "Worked Example 5" (Page 2 of 6) PLAN AND CROSS-SECTION **SECTION:** 1-1 (Most Severe Consequence) 0 2-2 (Maximum Feature Height) (1)220 UC Crack of slope cover due to tree growth 220 UC Possible failure scar PLAN (Not to scale)

- Notes:
  PLAN (1:1000)

  1. Feature boundary (SIS) and Revised Feature Boundary (if applicable)
  2. Section Mark
  3. Photo Location and Direction
  4. Signs of distress, if any

- 5. Signs of seepage, if any6. Engineering measures (e.g. thickening & skin walls)

- CROSS-SECTIONS

  1. Fully dimensioned
  2. Existing engineering measures. (e.g. thickening & skin walls)

### FEATURE NO. "Worked Example 5"

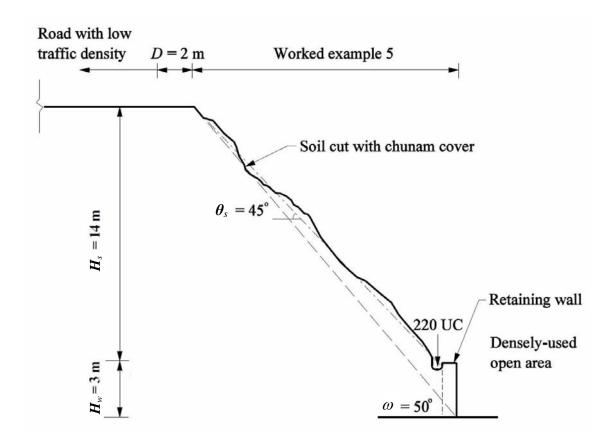
(Page 3 of 6)

### PLAN AND CROSS-SECTION

**SECTION:** 

1-1 (Most Severe Consequence)

0 2-2 (Maximum Feature Height)



Note: No reinforcement or structural support observed on site

### Section 1-1 (Not to scale)

- Feature boundary (SIS) and Revised Feature Boundary (if applicable)
- Section Mark

- Photo Location and Direction
  Signs of distress, if any
  Signs of seepage, if any
  Engineering measures (e.g. thickening & skin walls)

### **CROSS-SECTIONS**

- Fully dimensioned
   Existing engineering measures. (e.g. thickening & skin walls)

FEATURE NO. "Worked	d Example :	5''				(Page 4 of 6)
WALL CHARACTERISTICS			SITE OB	SERVATIONS/FINDING	GS	
Wall Type	<ul> <li>○ Random rubble masonry wall</li> <li>○ Brickwall</li> <li>○ Wall composed of lime stabilized soil</li> <li>○ Dry-packed dressed block or squared rubble wall</li> <li>□ with ties</li> <li>□ without ties</li> <li>○ Masonry wall other than random rubble wall</li> <li>□ with horizontal beam(s) made of concrete</li> <li>□ with horizontal beams(s) made of lime-soil or brick</li> <li>□ without horizontal beam(s)</li> <li>✓ Concrete wall (with or without masonry facing)</li> <li>○ Others:</li></ul>					
Base Width, B <sub>W</sub>	Base Width mm as determined from  O Documentary records (Thickness Gauging/EI/MM/As-built drawings)  Weephole Probing (Provide field weephole probing record on Page 5)  ✓ Others: cannot be determined from above, accord H <sub>e</sub> /B <sub>w</sub> = 5					
Slope Protection	Surface cover with  O Vegetation					
	Location	Size (mm)	Spacing (m)	Type (e.g. U-channel, step channel, downpipes or ditch)	Adequate Capacity (Y/N)	Remarks
	Crest	220		U-channel	Y	
	Berm					
Surface Drainage Provision	On Slope					
	o Feature Inadequ	ed or infer located or ate surfac	rred from top n a drainage ee drainage e	nverge onto the crest pographic plan or aerial ph line/zone of depression vident by surface erosion	otos) or erosion gul	

FEATURE NO. "Work	ed Example 5''			(Page 5 of 6)
WALL CHARACTERISTICS	SITE	E OBSERVATIO	NS/FINDINGS	
	Signs of Seepage?		o Yes	<b>√</b> No
	If Yes, provide following det	ails 	Condition of seepa	~~
Signs of Seepage	Seepage Location	Copious	Trickling/damp	Stain
	At or above mid-height	_		
	Below mid-height			
	o Others:			
	Indicate seepage location on	plan and sections	S	
Water-carrying Services	Indication of presence of unde  Valve(s) of water main w  Manhole cover(s) within  Others:  Signs of leaking?  Yes  If Yes, indicate location and co	ithin crest area/o crest area/on the	n the wall wall	
Signs of Distress  (Provide photographic records of signs of distress and indicate location & extent on plan & cross-sections)	<ul> <li>Reported signs of distress</li> <li>Observed signs of distress</li> <li>Deformation of the Wall</li> <li>Long continuous crack width</li> <li>Sub-vertical through Crack width</li> <li>Bulging of wall face Horizontal distance and the wall toe =</li> <li>Fabric condition of rubble General intact without Cocalised mortar/points</li> <li>Missing mortar/points</li> </ul>	(please tick)  ck at wall crest so mm, equivalent crack in return volume mm measured a between the vert mm  e/masonry wall ut signs of distresonting missing	ub-parallel to wall; t to % of wal vall at m above toe ical line from the pe	l height
	o Minor dislocation of	_		
	o Some blocks missing	g or dislocated		
	Where severe signs of follow-up action should be			noted, appropriate
	Judgment should be mad cracking) are induced du     In the latter circumstance	ring wall constru	action or due to inad	equate maintenance.

FEATURE NO. "Worked ]	Example 5''	(Page 6 of 6)
WALL CHARACTERISTICS	SITE OBSERVATIONS/FINDINGS	
Instability after Wall Formation/Treatment  (Provide photographic records of the inferred failure scar and indicate location on plan & cross-sections)	<ul> <li>✓ No indication of any failure occurred after formation or treatment</li> <li>○ Reported failure of the wall</li> <li>○ Possible failure scar observed at of the wall</li> <li>Estimated failure volume = m³</li> <li>○ Debris observed on site/Other observations:</li> </ul>	
OTHER OBSERVATIONS/REM	nta collection sheets for soil cut slope portion	
	/ 06 / 2009 (dd/mm/yyyyy) BY: PAI	

## **E.4** Worked Example (*TS* Computation Sheets - Soil Cut Portion)

FEA	TURE NO. "Worked Example 5"	SECTION:		st Severe Consequence) kimum Feature Height)
(A)	INSTABILITY POTENTIAL (IP)			
(A1)	Year of Formation/Treatment (Y)		<u>A1</u>	
	<ul> <li>(i) Y≤1980</li> <li>(ii) 1980 &lt; Y≤1990</li> <li>(iii) 1990 &lt; Y≤1995</li> <li>(iv) Y&gt;1995</li> </ul>		6 4 2	A1 <b>6</b>
	For soil cut slopes excluded from ranking (see	e Note 8), denote $AI = 0$	-	
(A2)	Level of Geotechnical Engineering Input  (i) Slopes with none or little geotechnical e  (ii) Slopes with indication of some geotechn  (iii) Slopes with indication of substantial geo  (iv) Slopes checked and accepted by GEO	nical engineering input	A2 8 6 out 2	A2 <b>8</b>
(A3)	(ii) Rock Slope Height, $H_r$ $0 \text{ m}$ (iii) Crest Wall Height, $H_{cw}$ $0 \text{ m}$ (iv) Toe Wall Height, $H_{tw}$ $3 \text{ m}$	Feature Height, H $H = H_s + H_r + H_{cw} + H_{$	0 m 0 m 14 m	*H <sub>r</sub> '= rock slope portion where a realistic slip surface daylights (see Note 14)
	(ix) Downslope Gradient, $\alpha$ 0 °			

Geometry Classification (refer to Fig	gure A2)		<u>A3</u>	
(i) S1 (ii) S2			8 4	
(ii) <i>S3</i>			2	
(iv) S4			1	A3 2
(IV) 34			1	
(A4) Slope Protection and Surface I	<u>Drainage</u>			
Slope Protection	Soil slope or	Soil slope or	Soil slope or	
Stope Protection	crest area substantially	crest area	crest area	
Surface Drainage	unprotected	partially protected	substantially protected	
Few or no channels, and potential for convergent flow of surface	8		2	
water above crest or located on a drainage line or depression	8	4	2	
Few or no channels	4	2	1.5	
Adequate channels	2	1.5	1	A4 1.5
Adverse geological	gical tings Significa	nt Moderate	Minor/None	
feature				
Significant	10	8	5	
Moderate	8	3	2	A5 1
Minor/None	5	2		
(B) ACTUAL PERFORMANCE	E (AP)			
(B1) Signs of Distress				
· · · · · · ·			<u>B1</u>	
(i) Severe (signs of slope movement	t)		10	
(ii) Moderate (extensive minor defects)			4	B1 <b>4</b>
(iii) Minor/None (none or few isolated min	nor defects)		1	

(B2)	Inst	ability after Slope Formation/Treatment			
(12)	11156	and area proper ormanon treatment	<u>B2</u>		
	(i)	Massive failures (> 500 m <sup>3</sup> )	10		
	(ii)	Major or repeated minor failures	5		
	(:::)	or records of previous severe signs of distress	f 1:-t 2		
	(111)	Minor failure or records of previous moderate sign	ns of distress 2		
	(iv)	No failure or records of previous minor signs of di	stress 1	B2	2
(C)	FAC	CILITIES ABOVE CREST OF FEATURE			
	(i)	Type of crest facility	Road with low	Facility	C1
		(for roads and footpaths, give also the name) (refer to Table 2.1 of the main text)	traffic density	Group	
		(lefer to fuote 2.1 of the main text)	J	1 (a)	9
	(ii)	Facility Group		1 (b)	3
	(11)	Tacinty Group	4	2 (a)	2
				2 (b)	1
	(iii)	Distance ( <i>D</i> ) from crest of feature to crest		3	0.25
	(111)	facility (refer to Figure 2.1 of the main text)	2.5 m	4	0.002
			2.0	5	0.0002
				C1	0.002
	(iv)	Vulnerability Factor, C2 (refer to Table 3.1 of the main text)		C2	0.4
<b>(D)</b>	FA(	CILITY AT TOE OF FEATURE			
	(i)	Type of toe facility		Facility	
	(1)	(for roads and footpaths, give also the name)	Densely-used	Group	D1
		(refer to Table 2.1 of the main text)	open area	1 (a)	9
				1 (b)	3
	(ii)	Facility Group	3	2 (a)	2
			3	2 (b)	1
				3	0.25
	/**··	5	0	4	0.002
	(111)	Distance ( <i>L</i> ) from toe of feature to toe facility (refer to Figure 2.1 of the main text)	0 m	5	0.0002
	(iv)	Shadow angle ( $\omega$ ) from crest of feature to toe facility (refer to Figure 2.1 of the main text)	49°	D1	0.25
	(v)	Vulnerability Factor, <i>D2</i> (refer to Table 3.2 of the main text)		D2	0.92

CALCULATED SCORES		
INSTABILITY SCORE (IS)		
$IS = A1 \times A2 \times A3 \times A4 \times A5 \times B1 \times B2$	IS	1152
CONSEQUENCE SCORE (CS)		
$CS = [C1 \times C2 + D1 \times D2] \times H$	CS	3.9236
TOTAL SCORE (TS)		
$TS = IS \times CS$	TS	4520.0

## **E.5** Worked Example (TS Computation Sheets - Retaining Wall Portion)

FEATURE NO. "Worked Example 5"			Severe Consequence) num Feature Height)
(A) INSTABILITY POTENTIAL (IP)			
(A1) <u>Level of Geotechnical Engineering Input</u>			
		<u>A1</u>	
(i) Features with none or little geotechnical engin	eering input	10	
(ii) Features with indication of some geotechnical	engineering input	3	
(iii) Features with indication of substantial geotech	nnical engineering inp	out 1	A1 10
For retaining walls excluded from ranking (see Note	7), denote $A1 = 0$		
(A2) Geometry (refer to Figure D1)			
Section 1-1 2-2_			
<b>\ m</b>     — m	ure Height, $H$ $H_s + H_r + H_w$	17 m	
	ctive Height, $H_e$		
Height, $H_r$ $0$ $\mathbf{m}$ $H_e =$	$H_w(1+0.35\tan\beta)+$	$\frac{s}{\gamma_b}$ 4.5 m	
(iii) Soil Slope Height, $H_s$ 14 m — m where $\gamma$	$b_0 = \text{soil bulk unit wei}$	ight $20 \frac{kN}{m^3}$	
(iv) Upslope Angle, $\beta$ 45 ° (xi) $H_{e'}$	$B_w =$	5	
(v) Wall Face Angle, $\theta_w$ 90 $^{\rm o}$ $-^{\rm o}$			
(vi) Surcharge at crest of wall, s   10 kPa  — kPa			
(vii) Base width, $B_w$ — m — m			
(viii) Average Wall Face Angle (in case of multiple walls), θ			

Classification (i) $H_e/B_w > 4.2$ (ii) $3.5 < H_e/B_w \le 4.2$ (iii) $2.8 < H_e/B_w \le 3.5$ (iv) $2.0 < H_e/B_w \le 2.8$ (v) $H_e/B_w \le 2.0$				A2 8 6 4 2 1	A2 <b>8</b>
(A3) Wall Type (refer to Figure 1	D2)				
Type of Wall			A3		
Random rubble masonry horizontal beams)	wall (with or wit	hout pointing, ties	or 8		
<ul> <li>Wall composed of lime-stab</li> <li>Brick Wall</li> <li>Dry packed dressed block/sc</li> <li>Any type of masonry wall horizontal beams made of line</li> </ul>	quared rubble wall	om rubble walls) w	5		
· -	<ul> <li>Dry packed dressed block/squared rubble wall with ties</li> <li>Any type of masonry wall (except for random rubble walls) with</li> </ul>		rith 3		
Masonry facing to concrete wall     Concrete wall		1		A3 1	
Other Wall Type					
(A4) Surface Protection and Surf	ace Drainage				
Surface Protection Surface Drainage	Crest area substantially unprotected	Crest area partially protected	Crest area substantially protected		
Few or no channels above wall crest, and potential for convergent flow of surface water above crest	8	4	2		
Few or no channels above wall crest	4	2	1.5		
Adequate channels	2	1.5	1		A4 1.5

### (A5) Signs of Seepage and Leaky Water-Carrying Services

FACILITIES ABOVE CREST OF FEATURE

**(C)** 

	Presence of potentially leaky services & signs of leakage noted	Presence of potentially leaky services but no signs of leakage noted	No potentially leaky services
Seepage at mid-height or above	8	4	2
Seepage below mid-height	4	2	1.5
No signs of seepage	2	1.5	1

1 A5

5

(B) AC	TUAL PERFORMANCE (AP)		
(B1) <u>Sig</u> (i)	Severe (Advanced stage of severe deformation and/or distress or	<u>B1</u> 10	
(ii)	onset of severe deformation and/or distress)  Moderate (Moderate deformation and/or distress)	4	
(iii)	Minor/None (Minimal deformation and distress)	1	BI 10
	r a wall of the slenderness ratio, $H_e/B_w \ge 5$ or a dry packed random oble wall with $H_w > 5$ m, accord $BI = 10$		
(B2) <u>Inst</u>	ability after Slope Formation/Treatment	R2	
(i)	Major (full-height failure)	<u>B2</u> 10	
(ii)	Multiple part-height or structural failures, or records of previous severe signs of distress	5	
(iii)	Part-height or structural failures, or records of previous moderate signs of distress	2	B2 <b>1</b>
(iv)	No failure nor records of previous signs of distress	1	

### Facility (i) Type of crest facility Road/footpath C1(for roads and footpaths, give also the name) Group with low traffic (refer to Table 2.1 of the main text) density 1 (a) 9 1 (b) 3 (ii) Facility Group 2 (a) 2 4 2 (b) 1 0.25 3 (iii) Distance (D) from crest of feature to the crest facility (refer to Figure 2.1 of the main text) 0.002 4 16 m 0.0002

Г			
		CI	0.002
(iv) Vulnerability Factor, C2 (refer to Table 3.1 of the main text)		C2 [	0
(D) FACILITY AT TOE OF FEATURE			
(i) Type of toe facility (for roads and footpaths, give also the name) (refer to Table 2.1 of the main text)	Densely-used open area	Facility Group 1 (a)	<i>D1</i>
		1 (b)	3
(ii) Facility Group	3	2 (a) 2 (b)	2
		3	0.25
		4	0.002
(iii) Shadow angle (a) from crest of feature to toe facility (refer to Figure 2.1 of the main text)	<b>49</b> °	5	0.0002
(iv) Distance (L) from toe of feature to toe facility (refer to Figure 2.1 of the main text)	0 m	D1	0.25
(v) Vulnerability Factor, D2 (refer to Table 3.2 of the main text)		D2 [	0.92
CALCULATED SCORES			
INSTABILITY SCORE (IS)			
$IS = A1 \times A2 \times A3 \times A4 \times A5 \times B1 \times B2$		IS	1200
CONSEQUENCE SCORE (CS)			3.91
$CS = [C1 \times C2 + D1 \times D2] \times H$		CS	3.71
		Г	
TOTAL SCORE (TS)			4692.0
$TS = IS \times CS$			

### **E.6** Worked Example (RS Computation)

### "WORKED EXAMPLE 5"

(A) Soil Cut Portion

$$TS = 4520.0$$

According to the equation in Appendix E.1

$$RS = 0.063 \times TS$$

= 284.8

(B) Retaining Wall Portion

$$TS = 4692.0$$

According to the equation in Appendix E.1

$$RS = 0.027 \times TS$$

= 126.7

(C) Combined RS

$$RS$$
 (soil cut) +  $RS$  (retaining wall) =  $284.8 + 126.7$ 

= 411.5

## Appendix F

Examples of Severe Signs of Distress



Example F1 Displaced Surface Channel



Example F2 Cracking of Berm



Example F3 Displaced U-channel



Example F4 Cracking and Bulging of Hard Cover



Example F5 Displaced Pipeline



Example F6 Displaced Surface Channel



Example F7 Deformed Railings



Example F8 Detached Surface Channel



Example F9 Cracking at Slope Crest



Example F10 Sheared Concrete Steps



Example F11 Cracking of Hard Cover



Example F12 Extensive Cracking of Hard Cover



Example F13 Voids Underneath Hard Cover



Example F14 Subsidence and Extensive Cracking of Hard Cover



Example F15 Wall Tilting



Example F16 Wall Cracking



Example F17 Tension Cracks



Example F18 Extensive Tension Cracks

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Geotechnical Manual for Slopes, 2nd Edition (1984), 302 p. (English Version), (Reprinted, 2011).

斜坡岩土工程手冊(1998),308頁(1984年英文版的中文譯本)。

Highway Slope Manual (2000), 114 p.

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岩土指南第五冊	斜坡維修指南,第三版(2003),120頁(中文版)。
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Geoguide 7	Guide to Soil Nail Design and Construction (2008), 97 p.

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### **GEOLOGICAL PUBLICATIONS**

The Quaternary Geology of Hong Kong, by J.A. Fyfe, R. Shaw, S.D.G. Campbell, K.W. Lai & P.A. Kirk (2000), 210 p. plus 6 maps.

The Pre-Quaternary Geology of Hong Kong, by R.J. Sewell, S.D.G. Campbell, C.J.N. Fletcher, K.W. Lai & P.A. Kirk (2000), 181 p. plus 4 maps.

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